

1 **Title:** Swimming with swimsuit and wetsuit at typical vs cold-water temperatures (26 vs
2 18°C)

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4 **Full Names of the Authors and Institutional/Corporate Affiliations:**

5 Ana Gay¹

6 Rodrigo Zacca^{2,3,4}

7 J. Arturo Abraldes⁵

8 Esther Morales¹

9 Gracia López-Contreras¹

10 Ricardo J. Fernandes^{2,3}

11 Raúl Arellano¹

12

13 ¹Aquatics Lab, Department of Physical Education and Sports, Faculty of Sport Sciences,
14 University of Granada, Granada, Spain.

15 ²Centre of Research, Education, Innovation and Intervention in Sport (CIFI2D), Faculty
16 of Sport, University of Porto, Porto, Portugal

17 ³Porto Biomechanics Laboratory (LABIOMEPE), Faculty of Sport, University of Porto,
18 Porto, Portugal.

19 ⁵Research Group Movement, Science and Sport, Faculty of Sport Science, University of
20 Murcia, Spain.

21

22

23 **Contact Details for the Corresponding Author:**

24 Ricardo J. Fernandes

25 Centre of Research, Education, Innovation and Intervention in Sport (CIFI2D), Faculty
26 of Sport, University of Porto, Porto, Portugal.

27 Porto Biomechanics Laboratory (LABIOMEPEP-UP), University of Porto, Porto, Portugal.

28 R. Dr. Plácido da Costa 91, 4200-450, Porto, Portugal.

29 Phone: +351 220425273

30 Email: ricfer@fade.up.pt

31

32 **ABSTRACT**

33

34 The study aimed to compare three swimming conditions in a swimming flume with water
35 at 26°C (using swimsuit) and 18°C (randomly with swimsuit and wetsuit). Seventeen
36 swimmers (32.4±14.7 years old, 175.6±0.06cm height, and 70.4±9.8kg body mass)
37 performed the three bouts until exhaustion at 400m front crawl pace (24h intervals).

38 ANOVA repeated measures compared the experimental conditions. Swimming at 26°C
39 with swimsuit evidenced a higher metabolic demand (total energy expenditure; (E)),
40 comparing to 18°C swimsuit (p=0.05) and with 18°C wetsuit (p=0.04). The 26°C swimsuit
41 condition presented higher peak oxygen uptake ($\dot{V}O_{2peak}$), blood lactate concentrations
42 ($[La-]_{peak}$), rate of perceived exertion (RPE), maximal heart rate (HR_{max}), anaerobic lactic
43 energy (AnL), E, energy cost (C), $\dot{V}O_2$ amplitude (Ap), and stroke rate (SR), but lower
44 stroke length (SL) and stroke index (SI) than 18°C wetsuit. The 18°C swimsuit condition
45 (comparing to wetsuit) lead to higher $\dot{V}O_{2peak}$, $[La-]_{peak}$, HR_{max} , E, C, Ap, and SR but
46 lower SL and SI. Swimming at aerobic power intensity with swim and wetsuit at 18°C

47 does not induce physiologic and biomechanical disadvantages comparing to 26°C, The
48 results suggested that the use of wetsuit might increase performance at 18°C water
49 temperature for competitive master swimmers. Thus, its use is recommended in open
50 water swimming competitions when the water temperature is 18-20°C.

51

52 **Key words:** Wet suit, Energetics, Biomechanics, Swimming Flume, Open water,
53 Neoprene.

54

55 INTRODUCTION

56

57 The use of wetsuit in open water swimming events is very frequent due to the
58 enhancement in speed compared to the use of swimsuit. The properties of a wetsuit
59 provoke an increase in buoyancy, leading to a reduction on hydrodynamic drag. It also
60 induce the increase in propelling efficiency (η_p) resulting in the decrease of the energy
61 cost of swimming (C) [1,2,3]. In fact, both former and contemporary studies showed a 5
62 to 7% of performance improvement on 400 m to 30 min swimming events when wearing
63 a wetsuit [1,4-6], probably due to body drag reduction caused by the buoyancy increment
64 [1]. However, there is a high variety of wetsuits models (full body, sleeveless long, and
65 short), some of which are more economic to swim with (presenting lower C values) than
66 others, related to the body cover [4,7,8].

67 The use of wetsuits in open water competitions is mandatory, allowed and forbidden
68 depending on water temperature (lower than 18, from 18 to 20, and higher of 20°C,
69 respectively) [9]. The reason is to avoid hypothermia in cold-water temperatures [10].
70 When the immersion in with cold-water lead to the “cold-shock” physiological
71 phenomenon that is characterized by 1-3 min of hyperventilation and tachycardia

72 followed by an inspiratory gasp and by a heart rate (HR) decrease due to a blood flow
73 volume reduction [11]. However, these responses are only observed when swimming at
74 temperatures $\leq 15^{\circ}\text{C}$ and in deep immersions [12,13] but it is not clarified if there are
75 physiologic and biomechanical modifications when swimming with a wetsuit at 18°C .
76 Open water swimming is different compared to pool swimming since there are no turns
77 and wall push-off glide, as the water volume is higher and water temperatures varies,
78 leading to particular cardiovascular and technical responses [14,15]. Therefore,
79 swimming in a flume at different water temperatures could be a good strategy to simulate
80 the typical continuous open water swimming both during training and testing. It was
81 recently observed that performing in a swimming flume and in a 25 m pool is
82 physiological and biomechanically different (independently of the suit used) [6]. In
83 addition, differences in fluid flow characteristics and the changes in their swimming
84 technique during continuous swimming might appear when fatigue occurs [16,17].
85 Knowing that the 400 m front crawl pace is well related with the velocity that elicits
86 maximal oxygen consumption ($\dot{V}\text{O}_{2\text{max}}$) and is a valid indicator of aerobic power (one of
87 the most important swimming training zones) in which the anaerobic contribution range
88 between 17 and 40% of the total energy expenditure [18,19], the aim of this study was to
89 compare swimming performed at two water temperatures (18 and 26°C) with and without
90 wetsuits. It was hypothesized that: (i) swimming with a swimsuit at 26 vs 18°C implies
91 lower physiological demands and higher ηp ; and (ii) swimming at 18°C with swimsuit is
92 less efficient and economic than performing with a wetsuit.. Water temperatures of 26 and
93 18°C were selected since they represent the usual value at indoor swimming pools and
94 the limit under which the use of wetsuit is mandatory in open water swimming
95 competitions [9].

96

97 **METHODS**

98

99 *Participants*

100 Seventeen competitive master swimmers (15 males and 2 females) voluntarily
101 participated in the current study. Their main physical and performance characteristics
102 were 32.4 ± 14.7 years of age, 175.6 ± 0.06 cm of height, 70.4 ± 9.8 kg of body mass,
103 181.1 ± 7.1 cm of arm span, 23.03 ± 2.35 kg/m² of body mass index, and 273 ± 130
104 International Swimming Federation (FINA) points of best competitive performance on
105 400 m freestyle performance in short-course, with a training time frequency ~8-10 h per
106 week. The Institutional Ethical Review Board approved the study design that has been
107 performed according to the Code of Ethics of the World Medical Association -
108 Declaration of Helsinki (project code: 125/CEIH/2016) and the study follows the ethical
109 standards in sport and exercise science research [20]. A written informed consent was
110 given by all participants.

111

112 *Experimental Design*

113 After a standard in-water warm up of 1000 m [6] at 26°C, subjects performed three front
114 crawl time-trials in a swimming flume (with 24 h rest in-between) at a water speed
115 simulating each swimmer 400 m front crawl pace (the best time obtained in a 400 m
116 freestyle competition). The distance selected was assumed to be an aerobic power pace
117 [18,19]. Due to specific constraints to cool down the water, subjects firstly swam at 26°C
118 using a swimsuit and, after the water temperature was decreased to 18°C, they randomly
119 and counterbalanced perform the trials with a personal swimsuit and wetsuit (2.24 ± 0.89 ,
120 2.87 ± 1.18 , and 2.64 ± 1.07 mm of upper limbs trunk and lower limbs thickness
121 accordingly to FINA rules). In the three conditions swimmers were asked to stay at the

122 center of the swimming flume and to continue swimming until they were not able to keep
123 the pace. Swimmers had previous experience in flume swimming, using a breathing
124 snorkel and a nose clip, and abstained to take stimulant drinks and practice exhaustive
125 exercise 48 h prior to the trials. The trials were conducted at the same time of day (at a
126 room with $24 \pm 1.5^\circ\text{C}$ air temperature and $51 \pm 2.7\%$ relative air humidity) and prior 24
127 h nutrition was controlled.

128

129 *Methodology*

130 Experimental trials were conducted in a 2.4 x 4.7 m Endless Pool (Elite Techno Jet Swim
131 7.5 HP, Aston PA, USA), with its flow speed measured at 0.30 cm depth using an FP101
132 flow probe device (Global Water, Gold River, CA) [21]. A K4b² (Cosmed, Rome, Italy)
133 breath-by-breath portable gas analyzer which allows the direct measurement of
134 respiratory and pulmonary gas exchange variables, being suspended at 1.8 m above the
135 water surface (Figure 1). The gas analyzer was attached to a low hydrodynamic resistance
136 respiratory snorkel and valve system (Aquatrainer, Cosmed, Rome, Italy) [14,22] and was
137 calibrated with 16% O₂ and 5% CO₂ concentration gases before each testing session. HR
138 was measured using telemetry (Polar Wearlink, Kempele, Finlandia) synchronized with
139 the portable gas analyzer. A surface and underwater cameras (Nikon Corporation, Japan
140 and Panasonic Full-HD HX-A500, Osaka, Japan), operating at 50 Hz and placed on the
141 swimming flume frontal and sagittal plans (respectively), were used to assess the
142 biomechanical variables (see below). A pre-calibrated space was used as a reference for
143 video analysis with one meter wide and 14 points used for calibrations, situated in the
144 center of the swimming flume [6].

145

146 Insert Figure 1

147

148 *Data Analysis*

149 $\dot{V}O_2$ data was analyzed using the VO₂FITTING open and free software [23], with a
150 mono-exponential model adjusting the best profile for the three experimental conditions
151 (equation 1):

$$\dot{V}O_2(t) = A_0 + H(t - TD_p) \cdot A_p(1 - e^{-(t-TD_p)/\tau_p}) \quad (1)$$

152 where $\dot{V}O_2(t)$ represents the relative $\dot{V}O_2$ at the time t , A_0 is the rest $\dot{V}O_2$ (the pre-
153 exercise last 2 min average), H represents the Heaviside step function and A_p , TD_p and
154 τ_p are the fast $\dot{V}O_2$ component amplitude, time delay and time constant (respectively)
155 [23]. $\dot{V}O_2$ values included only those between $\dot{V}O_2 \pm 4$ SD, decreasing the noise between
156 breaths caused when swimmers swallow water, cough or the signal is interrupted [24].
157 Then, individual breath-by-breath $\dot{V}O_2$ responses were smoothed using a three-breath
158 moving average and time averaged every 10 s [23,24] allowing the highest incidence of
159 $\dot{V}O_2$ plateau occurrence regardless the distance performed [24]. Peak oxygen
160 consumption ($\dot{V}O_{2peak}$) and other physiological variables, as maximal heart rate (HR_{max})
161 and respiratory exchange ratio (RER), were obtained from the last 30 s of each trial.
162 The total energy expenditure (E) was estimated as the sum of aerobic (Aer), anaerobic
163 lactic (AnL) and anaerobic alactic (AnAL) energy contributions, with the first two
164 calculated, respectively, from the time integral of the net $\dot{V}O_2$ vs time relationship and
165 using the following equation [25,26]:

$$AnL = [La^-]_{net} \cdot \beta \cdot M \quad (2)$$

166 where $[La^-]_{net}$ is the difference between the blood lactate concentration ($[La^-]$) before and
167 after exercise ($[La^-]_{peak}$), β is the constant for O₂ equivalent of $[La^-]_{net}$ (2.7 ml · kg · min⁻¹)
168 and M is the swimmer body mass in kilograms. Afterwards, these energy contributions
169 were expressed in kJ assuming an energy equivalent of 20.9 kJ · L⁻¹ [19]. The AnAL was

170 estimated from the maximal phosphocreatine splitting in the contracting muscle, using
171 this equation [25]:

$$\mathbf{AnAL} = \mathbf{PCr} \cdot (1 - e^{-t/\tau}) \cdot \mathbf{M} \quad (3)$$

172 where PCr is the rest phosphocreatine concentration, t is the exercise time, τ is the PCr
173 splitting time constant at exercise onset (23.4 s) and M is the body mass. Then, AnAL
174 was expressed in kJ by assuming an energy equivalent of 0.468 kJ · mM and a
175 phosphate/oxygen ratio of 6.25 [27]. C was obtained as the ratio between E and distance
176 swam at 400 m front crawl pace [28]. Capillary blood samples (25 μ L) were collected
177 from the fingertip immediately after each trial (and at the 1, 3, 5 and 7 min of the recovery
178 period) using a portable lactate analyzer (Lactate Pro analyzer, Arkray, Inc., Kyoto,
179 Japan) to assess $[La^-]_{peak}$ [6,29]. In addition, immediately after each trial, swimmers rated
180 their perceived exertion (RPE) on a Borg scale [24].

181 Stroke rate (SR) was obtained measuring three consecutive upper limbs cycles, stroke
182 length (SL) was calculated from the ratio between v and corresponding SR [14] and stroke
183 index (SI), a measure of swimming efficiency, was calculated by multiplying v by SL
184 [19]. Finally, η_p was estimated as follow [30]:

$$\eta_p = [(v \cdot 0.9 / 2\pi \cdot SR \cdot l) \cdot 2/\pi] \cdot 100 \quad (4)$$

185 where l is the distance between the shoulder and wrist during the insweep (with the hand
186 situated exactly under the shoulder) Reference points were drawn at the shoulders, hips
187 and wrists to allow a proper biomechanical analysis. The distance between the points
188 were calculated with 2D motion analysis software Kinovea (version 0.8.15). For both
189 upper limbs due to a mirror was use to digitalize the upper limb of the left side of the
190 swimming flume.

191

192 *Statistical Analysis*

193 IBM SPSS Statistics (version 20, IBM SPSS, Chicago, USA) was used to data analysis,
194 with Shapiro-Wilk confirming its normality and homogeneity. ANOVA repeated
195 measures was computed to compare the three experimental conditions. Sphericity was
196 verified by means of the Mauchly test and adjusted according to the Greenhouse-Geisser
197 procedure when the significance of the F-ratios were not met. Bonferroni post hoc was
198 performed to locate the pairwise differences between the means ($p < 0.05$) with 95% of
199 confidence interval (CI). The Cohen's d effect was calculated (0 to 0.19 trivial, 0.2 to
200 0.59 small, 0.6 to 1.19 moderate, 1.2 to 1.99 large, 2.0 to 3.9 very large and > 4.0 nearly
201 perfect) [6]. The relationships between the time endured in the different trials and the
202 corresponding energetic contributions were assessed with Pearson's correlations
203 coefficients (r) and linear regression analysis.

204

205 **RESULTS**

206

207 Comparisons between experimental conditions conducted at different temperatures and
208 swimming suits at the 400 m front crawl pace are presented in Table 1. Bonferroni post
209 hoc analysis showed that E was different between the three comparisons. Nevertheless,
210 $\dot{V}O_{2peak}$, HR_{max} , $[La-]_{peak}$, C, Ap, SR, SL, and SI were different in between 26 swimsuit
211 and 18°C swimsuit and between 18 swimsuit and 18°C wetsuit conditions (Table 2). In
212 Table 1 it could be observed the percentual contribution of each energy system for the
213 overall swimming performance at each water temperature and suit condition. However,
214 only the AnL contribution showed differences between 26 swimsuit and 18°C wetsuit
215 conditions (Table 2). Complementarily, in the 26°C swimsuit condition, the time endured
216 at the aerobic power pace was directly related with Aer ($r = 0.69$; $p < 0.001$; Figure 2,
217 panel C) and inversely related with AnAL ($r = -0.62$; $p < 0.001$; Figure 2, panel A). No

218 statistically relationships were observed between swimming performance and energetic
219 contributions in the two other studied conditions (18°C swimsuit and 18°C wetsuit) as it
220 is shown in Figure 2.

221

222 Insert Table 1

223 Insert Table 2

224 Insert Figure 2

225

226 **DISCUSSION**

227 The main aim of the current study was to assess relevant physiological and biomechanical
228 variables while swimming to exhaustion at each individual 400 m front crawl pace (i.e.,
229 at the aerobic power intensity) using swim and wetsuits at typical and cold-water
230 temperatures. Contrary to our expectation, swimming with a swimsuit at 18°C did not
231 increase swimmers physiological demands (even enduring 20-25 s longer) compared to
232 performing at representative swimming pool water temperature (26°C). Additionally, as
233 anticipated, swimming at 18°C with swimsuit was less economic than with wetsuit (and
234 lower physiological variables values and better technical characteristics were observed in
235 this latter condition) accordingly with previous reports of better performances when
236 wearing wetsuits [1,4,6].

237 As referred before, using a wetsuit at open water competitions with 18°C water
238 temperature is optional [9]. It is known that subjects submerged in cold-water suffer a
239 cold-shock response that might lead to vasoconstriction and blood flow reduction [11],
240 particularly when using regular swimsuits that do not give any relevant protection against
241 low water temperatures. However, only RPE and E showed differences between the 26
242 and 18°C swimsuit conditions. The reason might be that this water temperature was not

243 sufficient to cause significant cold-shock responses and/or the exposure time was enough
244 to reduce the metabolic responses of cold water (which is studied to be subsided after the
245 first 5 min of immersion time [31]) and in the current study, the maximum time swam at
246 18°C water temperature was ~6.40 min. Still, when using a wetsuit at 18°C, an evident
247 decrease of the cardiorespiratory and technical variables was found, evidencing that this
248 condition required lower E and C values compared to 18° swimsuit as it can be observed
249 in Table 2 ($p = 0.04$; $d = 0.67$ and $p = 0.04$; $d = 0.68$, respectively) (i.e., it was more
250 economic than swimming with a swimsuit both at 26 and 18°C).

251 Regarding oxygen kinetics at the primary cardiorespiratory response, it was observed that
252 τ_p was > 20 s (as reported before [32]), with no differences between the three experimental
253 conditions. TDp also was similar between conditions, with values ~10-20 s. However, the
254 higher Ap values for the conditions 26°C swimsuit vs 18°C wetsuit and 18°C swimsuit vs
255 18°C wetsuit might indicate that the Aer contribution was accentuated by cold water and
256 wetsuit use. In addition, the AnL contributions were higher at 26 compared to 18°C
257 wetsuit, in accordance with the $[La^-]_{peak}$ values, an indicator of anaerobic energy
258 requirement [27]. This, plus the use of wetsuit in the cooler condition, might justify why
259 swimmers were able to maintain the time endured in all experimental conditions. When
260 swimming at 18°C without wetsuit, swimmers maintained the pace eventually due to the
261 cold-shock response that lead to higher HR_{max} values [11].

262 In fact, when wearing a wetsuit, swimmers lower limbs sinking torque is less expressive,
263 decreasing their hydrodynamic drag and, consequently, the C for the same speed [33].
264 This was observed in the current study with a SL and SI increment (and a SR decrease)
265 at the 18°C wetsuit condition even if usually the wetsuit thickness limits the shoulder
266 range of motion leading to a SR increase [34]. This is in line with previously reported
267 data when using a wetsuit comparing to swimsuit in a flume at the aerobic power intensity

268 [6]. As time to exhaustion at $\dot{V}O_{2max}$ is directly influenced by C, SL and SI [17,18,33],
269 the lower values in time endured at 26°C swimsuit seems to express that swimmers
270 experienced it as the most difficult metabolic and technical condition. This can be
271 observed by the higher RPE, $[La-]_{peak}$, $\dot{V}O_{2max}$, and SR values (also with higher values
272 of power), although the learning effect might also influenced the results since the warmer
273 condition was performed first.

274 In accordance with these data, a swimming efficiency rise at the 18°C wetsuit exertion
275 was expected. However, when comparing the η_p at the different conditions, the p value
276 although very close to 0.05 fell short of statistical meaning (with lower η^2 and power).
277 This might be justified by methodological constraints, particularly by the fact that the η_p
278 calculation was limited to the SR, neither considering technical aspects responsible for
279 propulsion nor thrust-producing vortices. Complementarily, the lower values of l might
280 have induced higher efficiency values [30], for which the swimming ability is an
281 important factor. Eventually, if another η_p assessment method was used (e.g., by
282 assessing the ratio of the speed of the center of mass to three dimensional speed of the
283 right and left upper limbs during underwater phase [29]) the results might be different.

284 It is also important to highlight that, even if a swimming flume allows to better set and
285 control the swimmers pace, it has some specificities that might influence both
286 physiological and biomechanical variables. In fact, the hydrodynamic resistance that
287 swimmers need to overcome is different from free swimming due to its non-laminar water
288 flow, consequently influencing swimmers technique and E [6,16]. The higher the water
289 temperature, the lower the water density and, consequently, the lower the hydrodynamic
290 resistance [35]. However, at higher temperatures the body temperature increases, and
291 more energy requirement might be necessary for self-regulation, probably explaining the
292 higher energetics requirement values at the 26°C condition.

293 Furthermore, flume swimming does not include the start and turn phases, which might
294 also influence swimmers E comparing to swimming in a pool. However, these swimmers
295 participate in open water and triathlon competitions hence, swimming in a flume might
296 replicate real swimming events. In addition, though our swimmers had considerable
297 experience using the swimming flume and the breathing snorkel, we could accept that
298 their technique might be affected and, in consequence, their energy requirements could
299 be different from swimming unimpeded in a pool, but as the aim of the study is related to
300 open water, the used of a swimming flume could be a more ecologically valid method to
301 measure continuous swimming than swimming pool. In conclusion, when using a wetsuit
302 at 18°C, an evident decrease of the cardiorespiratory and technical variables was found,
303 demonstrating that this condition require lower E and C values. Thus, it was more
304 economic than swimming with a swimsuit both at 26 and 18°C. The results suggested that
305 the use of wetsuit might increase performance at 18°C water temperature for competitive
306 master swimmers.

307

308 **PRACTICAL APPLICATIONS**

309

310 In the current study it was underscored the importance of the use of wetsuit at 18°C for
311 open water swimming competitions since it allows a better technique and effort economy
312 (comparing to wearing a swimsuit), meaning that for the same energy input its use will
313 allow better performances. Also, since the anaerobic threshold pace happens at ~90% of
314 the 400 m intensity [18,19], the physiologic and biomechanical variables values displayed
315 in our study could be useful for evaluating the open water swimmers and triathletes
316 performance that typically happens below or at that boundary [14,15]. Notwithstanding
317 the swimming flume particularities (that should be considered when analysing data), its

318 use makes the process of evaluating swimmers easier both at the physiologic and
319 biomechanical areas, reason why swimmers in general (and open water specialists in
320 particular) should use it on a regular basis to follow-up their training process.

321

322 **CONFLICT OF INTEREST**

323

324 Authors have no conflict of interest to report.

325

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438 TABLES AND FIGURES CAPTIONS

439 **Table 1.** Mean \pm SD, effect sizes, and power values of the comparison between the three
 440 different conditions (n = 17).

Variable	26° swimsuit	18°C swimsuit	18°C wetsuit	Time effect			
	Mean \pm SD	Mean \pm SD	Mean \pm SD	F	P	Eta ²	Power
Time endured (s)	304.91 \pm 78.38	330.83 \pm 52.97	334.11 \pm 52.13	1.58	0.22	0.09	0.31
v (m · s⁻¹)	1.23 \pm 0.21	1.23 \pm 0.17	1.24 \pm 0.21	0.44	0.55	0.03	0.10
VO_{2peak} (mL · kg⁻¹ · min⁻¹)	47.70 \pm 11.80 [†]	44.70 \pm 8.40 ^β	39.10 \pm 8.30 ^{†β}	12.64	0.00	0.44	0.99
VE (l/min⁻¹)	129.60 \pm 31.10 [†]	119.70 \pm 32.70	101.00 \pm 26.70 [†]	9.08	0.00	0.36	0.96
ΔVE (l/min⁻¹)	125.80 \pm 30.60 [†]	114.90 \pm 33.40 ^β	95.10 \pm 27.40 ^{†β}	10.72	0.00	0.40	0.98
[La⁻]_{basal} (mmol · l⁻¹)	2.25 \pm 0.78	2.22 \pm 1.08	2.18 \pm 1.14	0.04	0.97	0.00	0.05
[La⁻]_{peak} (mmol · l⁻¹)	10.25 \pm 3.45 [†]	7.99 \pm 4.38 ^β	5.21 \pm 2.65 ^{†β}	14.36	0.00	0.47	1.00
Δ[La⁻] (mmol · l⁻¹)	8.00 \pm 3.53 [†]	5.77 \pm 4.39	3.03 \pm 2.68 [†]	12.57	0.00	0.44	0.99
RPE	7.12 \pm 1.32 ^{*†}	5.35 \pm 1.73 [*]	6.00 \pm 2.09 [†]	9.38	0.00	0.37	0.97
HR_{max} (beats · min⁻¹)	181.88 \pm 19.24 [†]	182.88 \pm 18.79 ^β	154.18 \pm 12.08 ^{†β}	15.98	0.00	0.50	0.99
ΔHR (beats · min⁻¹)	105.47 \pm 18.39 [†]	109.76 \pm 21.71 ^β	74.12 \pm 15.14 ^{†β}	21.32	0.00	0.57	1.00
RF (breaths · min⁻¹)	57.98 \pm 19.27	51.61 \pm 13.92	51.43 \pm 15.76	2.12	0.14	0.12	0.40
ΔRF (breaths · min⁻¹)	50.63 \pm 19.90 [†]	43.33 \pm 14.36	41.43 \pm 16.12 [†]	3.70	0.04	0.19	0.64
RER	1.20 \pm 0.20	1.30 \pm 0.30	1.20 \pm 0.30	0.69	0.51	0.04	0.16
ΔRER	0.50 \pm 0.20	0.40 \pm 0.30	0.40 \pm 0.30	2.34	0.11	0.13	0.44
AnAL (kJ)	29.25 \pm 4.08	29.25 \pm 4.09	29.25 \pm 4.09	1.72	0.20	0.10	0.24
AnL (kJ)	31.72 \pm 14.73 [†]	23.06 \pm 18.78	12.18 \pm 11.01 [†]	12.99	0.00	0.45	0.99
Aer (kJ)	309.47 \pm 97.08	314.02 \pm 66.20	273.59 \pm 57.60	2.43	0.10	0.13	0.45
AnAL (%)	8.69 \pm 3.38	8.20 \pm 1.48	9.60 \pm 2.43	1.98	0.16	0.11	0.38
AnL (%)	8.60 \pm 3.54 [†]	6.15 \pm 4.15	3.88 \pm 3.34 [†]	12.20	0.00	0.43	0.99
Aer (%)	82.72 \pm 5.38	85.65 \pm 4.36	86.52 \pm 4.63	4.23	0.02	0.21	0.70
E (kJ)	370.44 \pm 105.88 ^{*†}	366.34 \pm 74.16 ^{*β}	315.02 \pm 60.71 ^{†β}	4.20	0.02	0.21	0.70
C (kJ · m⁻¹)	0.93 \pm 0.26 [†]	0.92 \pm 0.19 ^β	0.79 \pm 0.15 ^{†β}	4.20	0.02	0.21	0.70
Ap (ml · kg⁻¹ · min⁻¹)	42.40 \pm 12.30 [†]	37.00 \pm 5.90 ^β	32.20 \pm 6.80 ^{†β}	15.87	0.00	0.50	0.99
TDp (s)	18.98 \pm 8.35	18.02 \pm 6.90	16.44 \pm 0.79	0.70	0.51	0.04	0.16
τp (s)	25.20 \pm 12.17	26.21 \pm 17.60	23.55 \pm 15.46	0.18	0.83	0.01	0.08
SR (Hz)	0.56 \pm 0.08 [†]	0.55 \pm 0.07 ^β	0.51 \pm 0.07 ^{†β}	19.99	0.00	0.56	1.00
SL (m)	2.25 \pm 0.43 [†]	2.28 \pm 0.38 ^β	2.48 \pm 0.48 ^{†β}	16.81	0.00	0.51	1.00
SI (m² · s⁻¹)	2.83 \pm 1.04 [†]	2.86 \pm 0.84 ^β	3.15 \pm 1.17 ^{†β}	8.45	0.00	0.35	0.95
ηp (%)	46.55 \pm 8.96	45.90 \pm 8.35	48.90 \pm 10.93	3.16	0.06	0.16	0.56

Swimming speed (v), maximal oxygen consumption (VO_{2peak}) ventilation (VE), delta ventilation (ΔVE), basal blood lactate concentrations ([La⁻]_{basal}), peak blood lactate concentrations ([La⁻]_{peak}), delta blood lactate concentrations (Δ[La⁻]), Borg rating of perceived exertion scale (RPE), maximal heart rate (HR_{max}), delta heart rate (ΔHR), respiratory frequency (RF), delta respiratory frequency (ΔRF), respiratory exchange ratio (RER), delta respiratory exchange ratio (ΔRER), anaerobic alactic, anaerobic lactic and aerobic contributions (AnAL, AnL and Aer), total energy expenditure (E), energy cost (C), amplitude, time delay and tau of the oxygen consumption (Ap, TDp and τp), stroke rate, length and index (SR, SL and SI) and propelling efficiency (ηp). ^{*},[†] and ^βDifferences between 26 vs 18°C swimsuit, 26°C swimsuit vs 18°C wetsuit and 18°C swimsuit vs wetsuit.

443 **Table 2.** Mean difference, coefficient intervals (CI), and effect sizes of the significant

Variable	Difference [95%CI]; %Δ	p	Effect size (d)
26 swimsuit vs 18°C swimsuit			
RPE	1.76 [0.81, 2.72]; -24.79%	0.000	1.16, Moderate
E (kJ)	4.11 [-59.93, 68.14]; -1.11%	0.050	0.04, Trivial
26 swimsuit vs 18°C wetsuit			
$\dot{V}O_{2peak}$ (mL · kg ⁻¹ · min ⁻¹)	8.62 [3.86, 13.39]; -18.07%	0.001	1.17, Moderate
VE (l/min)	28.57 [11.41, 45.73]; -22.05%	0.001	1.08, Moderate
ΔVE (l/min)	30.71 [14.05, 47.36]; -24.41%	0.000	1.20, Large
[La] _{peak} (mmol·l ⁻¹)	5.04 [3.09, 6.99]; -49.2%	0.000	1.68, Large
Δ[La] (mmol·l ⁻¹)	4.97 [2.93, 7.02]; -62.13%	0.000	1.58, Large
RPE	1.12 [0.02, 2.21]; -15.7%	0.045	0.66, Moderate
HR _{max} (beats·min ⁻¹)	27.70 [14.60, 40.81]; -15.23%	0.000	1.37, Large
ΔHR (beats·min ⁻¹)	31.35 [16.95, 45.75]; -29.72%	0.000	1.41, Large
ΔRF (breaths·min ⁻¹)	9.2 [-0.26, 18.65]; -18.17%	0.050	0.63, Moderate
AnL (kJ)	19.54 [11.56, 27.52]; -61.6%	0.000	1.59, Large
AnL (%)	4.72 [2.24, 7.19]; -54.87%	0.000	1.24, Large
E (kJ)	55.42 [-1.25, 112.09]; -14.96%	0.050	0.63, Moderate
C (kJ · m ⁻¹)	0.14 [0, 0.28]; -14.96%	0.050	0.63, Moderate
Ap (ml · kg ⁻¹ · min ⁻¹)	10.1 [4.98, 15.23]; -23.86%	0.000	1.28, Large
SR (Hz)	0.05 [0.02, 0.08]; -8.68%	0.001	1.21, Large
SL (m)	-0.23 [-0.37, -0.1]; 10.39%	0.001	-1.11, Moderate
SI (m ² ·s ⁻¹)	-0.32 [-0.51, -0.14]; 11.33%	0.001	-1.11, Moderate
18 swimsuit vs 18°C wetsuit			
$\dot{V}O_{2peak}$ (mL · kg ⁻¹ · min ⁻¹)	5.62 [1.22, 10.03]; -12.57%	0.011	0.83, Moderate
ΔVE (l/min)	19.8 [0.44, 39.17]; -17.24%	0.044	0.66, Moderate
[La] _{peak} (mmol·l ⁻¹)	2.79 [0.15, 5.43]; -34.88%	0.037	0.69, Moderate
HR _{max} (beats·min ⁻¹)	28.70 [11.24, 46.18]; -15.69%	0.001	1.07, Moderate
ΔHR (beats·min ⁻¹)	35.64 [18.24, 53.06]; -32.47%	0.000	1.33, Large
E (kJ)	51.31 [2.02, 100.6]; -14.01%	0.040	0.67, Moderate
C (kJ · m ⁻¹)	0.13 [0.01, 0.25]; -14.01%	0.040	0.68, Moderate
Ap (ml · kg ⁻¹ · min ⁻¹)	4.76 [2.09, 7.43]; -12.86%	0.001	1.16, Moderate
SR (Hz)	0.04 [0.02, 0.05]; -6.83%	0.000	1.86, Large
SL (m)	-0.2 [-0.31, -0.09]; 8.59%	0.001	-1.15, Moderate
SI (m ² ·s ⁻¹)	-0.3 [-0.57, -0.02]; 10.34%	0.034	-0.70, Moderate

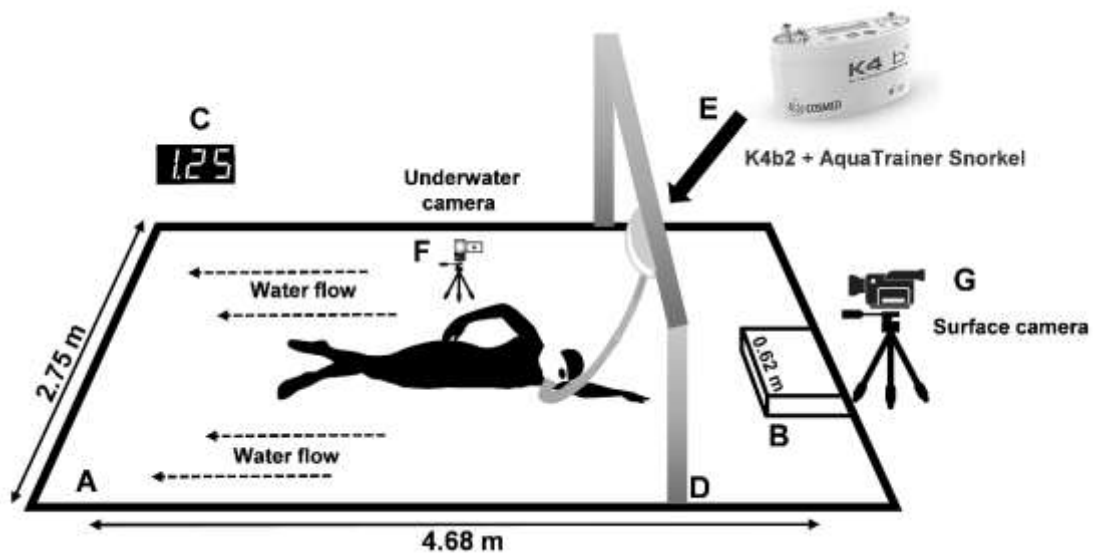
Borg rating of perceived exertion scale (RPE), total energy expenditure (E), Maximal oxygen consumption ($\dot{V}O_{2peak}$), ventilation ($\dot{V}E$), delta ventilation ($\Delta\dot{V}E$), peak blood lactate concentrations ([La]_{peak}), delta blood lactate concentrations ($\Delta[La]$), maximal heart rate (HR_{max}), delta heart rate (ΔHR), delta respiratory frequency (ΔRF), anaerobic lactic contribution (AnL), energy cost (C), amplitude of the oxygen consumption (Ap), stroke rate, length, and index (SR, SL and SI).

444 pairwise comparisons (n = 17).

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451 **Figure 1.** Graphic representation of the swimming flume. A: space for the swimmer; B:
452 water channel; C: flume monitor where it was selected the swimming speed; D: mobile
453 structure attached to the apparatus; E: K4b² and respiratory snorkel Aquatrainer; F:
454 underwater sagittal camera; and G: surface front camera. Dashed arrows represent the
455 water flow direction.

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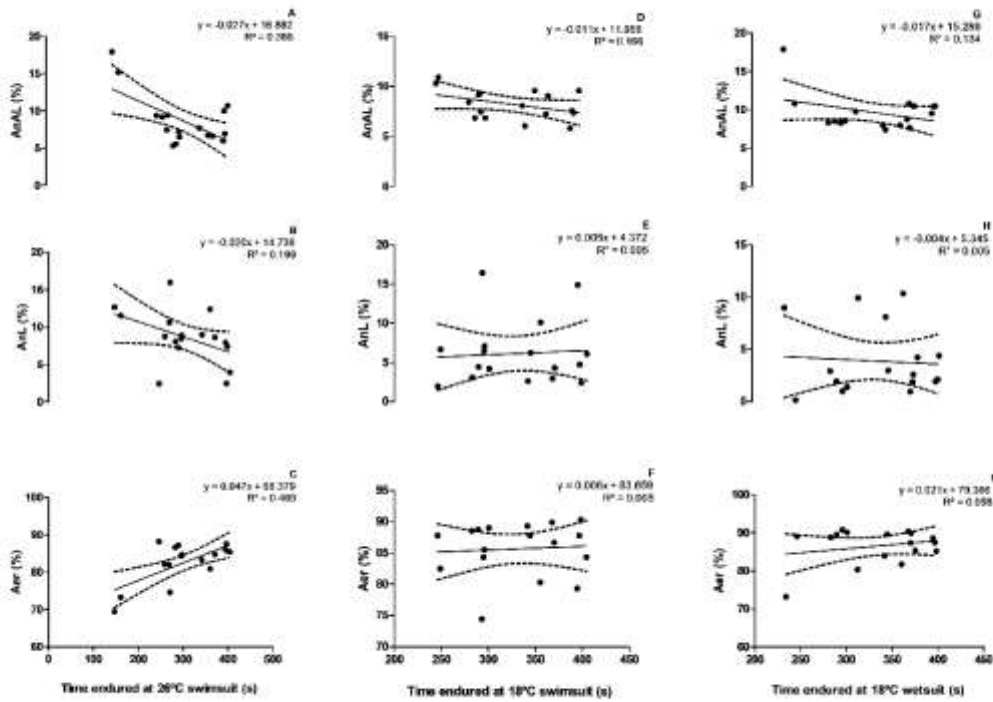
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467 **Figure 2.** Relationships between the times endured on 400 m front crawl (at 26 and 18°C
 468 with swimsuit and at 18°C with wetsuit) with the energetic contribution percentages.
 469 Anaerobic alactic energy (AnAL; panels A, D, and G); Anaerobic lactic energy (AnL;
 470 panels B, E, and H) and; Aerobic energy (Aer; panels C, F, and I). Individual values
 471 (continuous lines) and 95% confidence intervals (dashed lines) are represented (n = 17).

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