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Kinetic modeling of advanced starch oxidation with ozone in basic solutions

Authors

Alejandro Ávila-Sierra, José M. Vicaria*, Juan F. Martínez-Gallegos, Sara Cañadas,

Encarnación Jurado-Alameda

Affiliation

Chemical Engineering Department, Faculty of Sciences, University of Granada, Avda.

* Revie

Fuentenueva, s/n, 18071 Granada, Spain

Corresponding author

* José M. Vicaria

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Starch; ozone; kinetic model; advanced oxidation process; semi-batch reactor

Abstract

The growing use of ozone (O_3) in the last years to clean and enhance the physicochemical properties of starches, widely used as additives in food, beverage, and pharmaceutical industries, calls for a better understanding of their oxidation process. High pH, however, decomposes O_3 rapidly, forming highly-oxidant radicals, thus increasing the complexity of the reaction system. In this study, a kinetic model for the ozonation reaction of starch in an alkaline medium was developed and experimentally validated. Firstly, the concentration of hydroxyl radicals (•OH) over the reaction time is evaluated through the degradation of pCBA (a probe compound) to later evaluate and model the oxidation process of starch based on Chemical Oxygen Demand (COD) measurements.

By using a semi-batch reactor containing alkaline solutions at pH=13, different O_3 concentrations (0-42.30 g/Nm³) and temperatures (20-60°C), a pseudo first-order kinetic model was proposed to model the pCBA-ozone reaction. This model estimates the •OH formation, being [•OH] constant and proportional to the O₃ continuous dose. Therefore, under the conditions studied, •OH is a non-limiting reactant independent of temperature. The activation energy was estimated at 14.2±2.1 and 14.5±0.6 KJ/mol for 21.15 and 42.30 gO₃/Nm³, respectively. Then, COD data were used to propose a kinetic model for ozone-starch oxidation in alkaline media, where besides O₃ concentration and temperature, starch concentration (600-1700 mg/L) was also varied. According to the results, higher temperatures and longer reaction times resulted in a greater COD reduction, being it more pronounced at lower initial starch concentration. The activation energy of the ozone radicals-starch reaction was estimated at 8.1±0.4 KJ/mol, being significantly lower than those reported for the reaction between pCBA and •OH.

Introduction.

The application of ozone (O₃), a powerful oxidant, has considerably increased in recent years. It is commonly used to remove pollutants from effluents (Wang and Bai, 2017) and purify water (Brodowska, Nowak, and Smigielski, 2018), but also to clean and disinfect food processing lines (Ávila-Sierra et al., 2020, 2021; Medina-Rodríguez et al., 2020) and other surfaces and environments, especially after the advent of the COVID-19 pandemic (Epelle et al., 2023), to preserve foods (Pandiselvam et al., 2019a) or eliminate odors (Pandiselvam et al., 2019b). As a disinfectant, ozone has several advantages over traditional disinfectants like chlorine (Pascual, Llorca, and Canut, 2007) since O₃ decomposes quickly into oxygen without leaving residues (Castanha, Matta Junior, and Augusto, 2017; Catal and Ibanoglu, 2014), preserving foods, and avoiding the presence of contaminants in process effluents. As a cleaning agent, O_3 is effective in removing fatty (Chang, Chung, and Han, 2001; Jurado-Alameda et al., 2012; Vicaria et al., 2016), proteinaceous (Jurado-Alameda et al., 2014) and starchy deposits (Ávila-Sierra et al., 2020) adhered to hard surfaces. The cleaning of these deposits commonly requires high temperatures and/or strong alkaline formulations (Vicaria et al., 2017). Recently, Ávila-Sierra et al. (2020, 2021) studied the removal of starch from stainless steel using an advanced ozone-based oxidation process in high alkaline media, where the formation of hydroxyl radicals seems to enhance both the cleaning performance and the biodegradability of the cleaning wastewaters, reducing their toxicity and Chemical Oxygen Demand (COD); however a kinetic study on the starch degradation with the ozone under such conditions was not performed and, as far as we know, there is no literature about it.

In the last years, the use of O_3 has also gained considerable popularity for enhancing the physicochemical properties of starches (Sivaranjania et al., 2021; Maniglia et al., 2021) as they are widely used as additives in food, beverage, and pharmaceutical industries. Previous works have studied the effect of ozone in starch-based solutions at different pH (3-10), temperatures, and reaction times, being ozone able to modify the carboxyl content, swelling power and water solubility of starches (Chan, Bhat, and Karim, 2009; Gozé et al., 2016; Maniglia et al., 2019); their carboxyl content increased at high pH, while their water solubility decreased (Pudjihastuti, Handayani, and Sumardiono, 2018). At 25°C, Klein et al. (2014) also evaluated the pasting properties and surface morphology of ozone-oxidized starches under different pH (3.5-9.5), where higher both pH and ozone concentration favored cross-linking between the depolymerized starch molecules. Clearly, these variations in starch properties show that ozone is an effective oxidizing agent for starches. However, there is very little research on the ozonation of starch at high temperatures in high alkaline media, where O₃ is quickly decomposed to yield radicals with stronger oxidizing power (Brodowska, Nowak, and Smigielski, 2018; Hien et al., 2020).

The oxidative action of ozone comes from two mechanisms: direct reactions with O₃, or indirect reactions with hydroxyl radicals (Wang and Bai, 2017; Ghuge and Saroha, 2018; Hien et al., 2020). Hoigné (1997) and Elovitz & Von Gunten (1999) defined the hydroxyl radical (•OH) as a highly reactive and nonspecific oxidant formed from the O₃ decomposition. Hydroxyl radicals have higher oxidizing power than ozone molecules, with a standard redox potential of 2.8 V versus 2.07 V (Boczkaj and Fernandes, 2017). Elovitz and von Gunten (1999) defined R_{et} as the ratio •OH/O₃ that increases with pH, reaching very high values around pH=9, suggesting that the O₃ concentration is very low compared to the •OH concentration at high pHs (Elovitz, von Gunten and Kaiser, 2000). The direct reaction of ozone with other substances is selective, whilst hydroxyl radicals show faster non-selective reactions, attacking both organic and inorganic compounds (Boczkaj and Fernandes, 2017). Due to the selectivity criterion, incomplete mineralization of compounds commonly occurs in direct ozone reactions, whereas hydroxyl radicals can cause complete mineralization (Ghuge

and Saroha, 2018; Boczkaj and Fernandes, 2017; Nawrocki and Kasprzyk-Hordern, 2010). As a result of the improved performance, advanced oxidation processes, AOPs, have become increasingly popular for wastewater treatment (Ghuge & Saroha, 2018) as they increase degradation capacity, reduce operational time and costs, and allow the elimination of recalcitrant pollutants (Ghuge and Saroha, 2018; Hien et al., 2020; Kasprzyk-Hordern, Ziolek, and Nawrocki, 2003). Among all the AOPs, Fenton/photo-Fenton processes, ozonation, wet air oxidation (WAO), electrocoagulation and photocatalytic oxidation are extensively used (Ghuge and Saroha, 2018). Considering ozone-based AOPs, hydroxyl radicals can be produced by using alkaline pH, UV, H₂O₂, catalytic and photocatalytic ozonation, nonthermal DBD plasma and ozonation combination with Fenton and photo-Fenton (Beltrán, 2004; Hama Aziz et al., 2018; Hama Aziz, 2019 Hien et al., 2020).

Therefore, there is a current need to better understand the oxidation process of starches using ozone at high temperatures in alkaline conditions to improve its application for starch modification and industrial cleaning. Since ozone chemistry is complex, measuring the concentration of ozone and radicals may require indirect analytical methods using probe compounds such as p-chlorobenzoic acid (pCBA) (Elovitz and von Gunten, 1999). In this study, COD monitoring was used for investigating the kinetic of the starch-ozone reaction in alkaline media, where the generation of hydroxyl radicals was assessed using pCBA. The influence of ozone concentration and temperature were evaluated during ozonation using a semi-batch reactor.

Materials and methods.

Materials.

Corn starch (Maizena®, 87.91 % cornstarch, 11,50 %, moisture, 0.29% fat, 0.3% protein) and 4-Chlorobenzoic acid 99% (pCBA; supplied by Across Organics[™]) were used in this work.

Ozonation Device.

A semi-batch reactor (**Figure 1**) with an integrated ozonation system was used for ozonation experiments. The device allows the modification of ozone concentration, solution type, and temperature. It is composed by a jacketed tank (1L of capacity), a peristaltic pump (Heidolph, model 5006) supplying a 60L/h recirculation flow, a thermostatically controlled bath (P-Selecta, model Ultraterm), and a gas diffuser. Ozone was generated *in situ* from an oxygen stream using an ozone generator (Peripherals COM-AD, Anseros Germany). By recirculating the solution, a constant composition is maintained. The ozone concentration in the ozone-oxygen flow was determined for each assay by an analyzer (Anseros, Ozomat GM-6000-PRO, Germany). The volumetric flow of the ozone-oxygen gas flow was 40 NL/h. The residual ozone was eliminated passing through washing flasks with 5% KI aqueous solution before being released into the atmosphere.

Ozonation of Starch Solutions.

Ozonation of aqueous alkaline starch solutions (600-1700 mg starch/L of NaOH solution pH13) was carried out in a semi-batch reactor for 120 minutes at different temperatures, ranging between 40–60°C, and an ozone concentration of 42.30 g/Nm³, applying ozone dosages between 0-0.47 g O_3/L . The thermostatically controlled semi-batch reactor was filled with 1.2 L of the starch solution. Then, an oxygen current was introduced for 20 minutes, before ozonation began. Samples of 1 mL were extracted periodically from

the tank. The residual ozone of the samples was eliminated by adding 0.2 mL of 0.2 g/L Na_2SO_3 aqueous solution. At least three repeats were performed per experimental run.

Evaluation of Chemical Oxygen Demand (COD).

The COD value was analyzed according to Ávila-Sierra et al. (2020). Solution samples of 1.5 mL were extracted periodically and added to 1.5 mL of distilled water and mixed with the reagent solution. The reagent solution was formed by mixing 0.08 g Hg₂SO₄ (Panreac), 4 mL of sulfuric acid reagent (10 g/L Ag₂SO₄ dissolved in H₂SO₄) and 1 mL of 0.5 N K₂Cr₂O₇ aqueous solution. The vials were stirred and placed into a digestor (150°C, 2h). After digestion, the vials were cooled down to room temperature. Absorbance was measured at 620 nm. COD measurements were obtained by a calibration curve at different concentrations of a 0.85 g/L KC₈H₅O₄ solution (Panreac, Spain).

Evaluation of Oxidizing Power: pCBA Method.

The measure of radical concentration in ozonated solutions was based on the pCBA method described in Elovitz and von Gunten (1999). A 10 mg/L of pCBA in NaOH aqueous solution (pH=13) was introduced in the semi-batch reactor, thermostatted at the temperature of interest. Then, an oxygen current was introduced in the pCBA solution for 20 min, before ozonation experiments. The variables analyzed were ozone concentration (0.00, 21.15 and 42.30 g/Nm³, corresponding to an ozone feed rate of 0, 0.846 and 1.692 g/h respectively) obtaining applied ozone dosages between 0-0.47 g O₃/L, temperature (20, 40, 50, 60°C), and time (0-80 min). To evaluate the radical concentration in the ozonated alkaline solution, samples of 5 mL extracted periodically from the reactor and the pCBA concentration was measured as a function of time by spectrophotometry (Cary 100 Bio UV–Visible, Varian) at 234 nm, using a calibration line (0-0.01 g pCBA/L). Experiments were performed at least three times.

Results and discussion.

As highlighted in the introduction, a high pH causes ozone to decompose rapidly, forming radicals. As a function of ozonation time, the concentration of hydroxyl radicals was firstly evaluated through the degradation of pCBA. Then, the process of starch oxidation was modeled using Chemical Oxygen Demand (COD) data.

Evaluation of the Concentration of Hydroxyl Radicals in Alkaline Medium.

Figure 2 shows the $[pCBA]/[pCBA]_0$ profiles as a function of both time and temperature at two ozone concentrations, 21.15 g/Nm³ (**Figure 2.a**) and 42.30 g/Nm³ (**Figure 2.b**). With increasing time and temperature, the concentration of pCBA decreases, decreasing faster at high ozone concentration. Elovitz and von Gunten (1999) predicted the ozone concentration using a first-order kinetic model. However, measuring the concentration of the hydroxyl radicals is more complex as the reactivity of radicals towards the water matrix leads to a minimal steady-state concentration, typically <10⁻¹² M. Notwithstanding, the •OH concentration can be measured indirectly by an •OH-probe compound such as p-chlorobenzoic acid (pCBA), which is used due to its low reactivity with ozone ($k_{O3/pCBA} \le 0.15$ M⁻¹s⁻¹) and rapid reaction with •OH radicals ($k_{OH/pCBA} = 5 \cdot 10^9$ M⁻¹s⁻¹) (Elovitz and von Gunten, 1999). Therefore, considering that ozone is mainly transformed into hydroxyl radicals (•OH) at high pH (Boczkaj and Fernandes, 2017), the reaction scheme for ozone decomposition and subsequent hydroxyl radical reaction with pCBA could be defined as:

$$O_3 \rightarrow \eta^{\bullet} OH$$
 (Eq.1)

•OH +pCBA
$$\xrightarrow{k_{pCBA}}$$
 Products (Eq.2)

where k_{pCBA} is the individual rate constant for the •OH-pCBA reaction. Then, the kinetic model for this reaction is defined as:

$$-\frac{d[pCBA]}{dt} = k_{pCBA} [pCBA] [^{\bullet}OH]$$
(Eq.3)

where t is the reaction time.

Elovitz, von Gunten, and Kaiser (2000) found that for each temperature and ozone dose, the ratio [$^{\circ}$ OH]/[O₃] remained constant over time, where $^{\circ}$ OH exposure was unaffected by either reaction temperature or pH, while O₃ exposure changed drastically, decreasing it as both temperature and pH increased. The fast O₃ decomposition at high pH (Gounden, Singh, and Jonnalagadda, 2019) along with uninterrupted O₃ gas flow into the alkaline solution leads to a continuous formation of hydroxyl radicals. Considering that hydroxyl radicals steady-state concentrations are usually very low, typically <10⁻¹² M, it could be initially assumed that [$^{\circ}$ OH] is constant for a fixed ozone continuous dose. Then, the integration of (Eq. 3) gives:

$$\ln \frac{[pCBA]}{[pCBA]_0} = -k_{pCBA} [\bullet OH] t \quad (Eq.4)$$

Applying (Eq.4) to the experimental results, $\ln([pCBA]/[pCBA]_0)$ shows a linear dependence over time as a function of both temperature and the initial O₃ concentration (r² values between 0.987-0.998; **Table 1**), suggesting that k_{pCBA} [•OH], and therefore [•OH], remains constant over the entire reaction for each temperature and O₃ concentration assayed, being [•OH] a non-limiting factor. Then, for each ozone dose evaluated, it is possible to estimate the activation energy (E_{a1}) and k0_{pCBA} [•OH] for the •OH-pCBA reaction, fitting the data to the Arrhenius equation using (Eq.5):

$$\ln(k_{pCBA}[\bullet OH]) = \ln(k0_{pCBA}[\bullet OH]) - E_{a1}/R T$$
(Eq.5)

 k_{pCBA} [•OH] vs. 1/T fits well (Figure 3), with r² values between 0.957-0.998. The use of the parameters calculated reproduces the experimental results in a suitable form as shown in Figure 2.

The E_{a1} values obtained for each ozone dose used are similar (14.2±2.1 and 14.5±0.6 KJ/mol for 21.15 and 42.30 g O₃/Nm³ respectively), finding analogous values to the results reported by Elovitz, von Gunten, and Kaiser (2000), where •OH reactions activation energies varied between 5 and 10 KJ/mol. According to **Figure 3** and (Eq.5), kO_{pCBA} [•OH] is

independent of temperature but depends on the gas ozone concentration. kO_{pCBA} [•OH] is directly proportional to the concentration of ozone in the gas flow (**Figure 4**), according to (Eq.6).

$$k0_{pCBA}[^{\bullet}OH] = 28.9[O_3]$$
 $r^2=0.9998$ (Eq.6)

Therefore, under the experimental conditions used, [•OH] is constant and proportional to the ozone dose, as it was previously assumed for (Eq. 4) deduction, and independent of temperature. In fact, a similar increase in the production of hydroxyl radicals with a raising ozone dose has been previously described by Ghuge (2018).

Kinetic Modeling of Starch Oxidation with Ozone in Basic Solutions.

Modeling the kinetic of ozonation of polysaccharides is complex. Previous research proposed a kinetic model to explain the depolymerization of κ -carrageenan by ozone using viscosity changes (Prasetyaningrum, Ratnawati, and Jos, 2017). In the present work, a model for the ozone-starch reaction in alkaline solution at high pH was proposed based on the COD measurements, being [St] (g/L) the starch concentration as a function of time, [St]₀ (g/L) the initial starch concentration, and k_{St} the kinetic constant for the reaction:

$$\alpha [St] + [^{\bullet}OH] \xrightarrow{H}^{*_{St}} Products$$
 (Eq.7)

$$-\frac{d[St]}{dt} = k_{St} [^{\bullet}OH] [St]^{\alpha}$$
(Eq.8)

$$COD(mg O_2/L) = 1.116 [St] (mg/L)$$
 (Eq.9)

The concentration of starch is proportional to the COD, allowing to evaluate simultaneously the pollutant load of the chemical solutions over time.

As previously demonstrated in section 3.1, for each O_3 dose, [•OH] was constant throughout the entire reaction at pH=13, being independent of temperature. Then, substituting (Eq.9) in (Eq.8) and considering α =1, its integration results in:

$$-\ln\frac{\text{COD}}{\text{COD}_{0}} = k_{\text{St}} \left[{}^{\bullet}\text{OH} \right] t$$
 (Eq.10)

If α is not equal to 1, then:

$$\frac{\text{COD}}{\text{COD}_0} = \left[1 + \left(\frac{1.116}{\text{COD}_0}\right)^{1-\alpha} (\alpha - 1) \text{ k}_{\text{St}} \left[^{\bullet}\text{OH}\right] t\right]^{\frac{1}{1-\alpha}} \quad (\text{Eq.11})$$

Applying Eq.(11) to the experimental results, the best fitting was obtained at α =0.3 (Figure 5). The COD/COD₀ ratio decreased as both ozonation time and temperature increased, being this reduction more pronounced at low initial starch concentrations. According to the kinetic model proposed, k_{St} [•OH] remains constant over the entire reaction at each temperature and starch concentration. Then, k_{St} [•OH] (Table 2) could be fitted to the Arrhenius equation:

$$\ln \left(k_{St} \left[{}^{\bullet}OH \right] \right) = \ln \left(k_{St0} \left[{}^{\bullet}OH \right] \right) - \frac{E_{a2}}{R} T (Eq.12)$$

Applying Eq.(12) ($r^2=0.993$), E_{a2} and k_{St0} [•OH] were determined, being 8.1±0.4 KJ/mol and 780.7±1.1 (L/mg St)^{-0.7} h⁻¹ respectively. These parameters fit the experimental results in a suitable form as shown in **Figures 5**. Comparing both models, •OH-starch and •OH-pCBA, the E_{a2} values estimated for the reaction between starch and •OH were lower than those estimated for the •OH-pCBA reaction.

Previous works have shown that ozone can modify the composition and structure of starch, given its ability to break the glucosidic bonds that bind glucose molecules, causing starch depolymerization, and oxidizing its hydroxyl and carbonyl groups to carboxyl groups (Castanha, Matta Junior, and Augusto, 2017; Catal and Ibanoglu, 2014). Similarly, it has been observed how hydroxyl radicals react with oligosaccharides and polysaccharides, being capable of breaking glucosidic bonds (Dai et al., 2017). The glucose oxidation by ozone generates different products, including acidic sugars, such as uronic (glucuronic acid), aldonic (gluconic acid) and aldaric acids (glucaric acid). The subsequent oxidation of these substances gives rise to other organic acids and compounds with fewer carbon atoms, the latter arising from their decarboxylation causing the release of CO_2 (Marcq et al., 2009). Analogously, successive oxidations of starch by hydroxyl radicals during its ozonation at alkaline pH are

foreseeable and would be justified by the observed reduction of COD (Figure 5), being this COD reduction also found in previous works on cleaning of starchy deposits (Ávila-Sierra et al., 2020; 2021). Likewise, these oxidations and depolymerizations may change the properties of starch after ozonation, e.g., gelatinization, pasting, retrogradation and solubility (Catal and Ibanoglu, 2014), likely affecting the cleaning process of starches.

<text>

Conclusions.

In this work, the concentration of hydroxyl radicals (•OH) over time is firstly evaluated through the degradation of pCBA (a probe compound) to later evaluate and model the ozonation process of starch in alkaline solutions based on Chemical Oxygen Demand (COD) measurements.

By using a semi-batch reactor containing alkaline solutions at high pH (pH=13), different O₃ concentrations (0-42.30 g/Nm³) and temperatures (20-60°C), a pseudo first-order kinetic model was proposed to model the pCBA-ozone reaction. This model estimates the •OH formation, being [•OH] constant and proportional to the O₃ continuous dose. Therefore, and under the conditions studied, •OH is a non-limiting reactant independent of temperature. The activation energy was estimated at 14.2±2.1 and 14.5±0.6 KJ/mol for 21.15 and 42.30 g O₃/Nm³, respectively. Then, a kinetic model for ozone-starch oxidation in alkaline media was proposed based on COD data. The best fit was obtained at α =0.3. According to the results, higher temperatures and longer reaction times resulted in a greater reduction of COD, which was more pronounced at lower initial starch concentration. The activation energy of the ozone-starch reaction was estimated at 8.1±0.4 KJ/mol, being significantly lower than those reported for the reaction between pCBA and •OH.

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Figures captions.

Figure 1. Scheme of a semi-batch reactor with an integrated ozonation system. The device is composed of a (1) jacketed tank, (2) peristaltic pump, (3) thermostatically controlled bath and (4) gas diffusor.

Figure 2 – Ozonation of pCBA solutions in semi-batch reactor. Influence of time and temperature. • 20°C, \circ 40°C, **=** 50°C, \Box 60°C. Ozone concentration: a) 21.15 g/Nm³, b) 42.30 g/Nm³ Lines show the model proposed.

Figure 3 – Dependence of k_{pCBA} [•OH] with temperature. Ozone concentration in oxygenozone current: • 21.15 g/Nm³, • 42.30 g/Nm³.

Figure 4 – Dependence of $k0_{pCBA}$ [•OH] with ozone dose.

Figure 5 – Ozonation of aqueous solutions of starch vs. temperature and time. pH=13. Starch concentration: ● 600 mg/L, ○ 1300 mg/L, ■ 1700 mg/L). (a) 40°C, (b) 50°C, (c) 60°C. — model proposed, Eq. (11). Bars errors show the standard deviation of three samples.



Figure 1. Scheme of a semi-batch reactor with an integrated ozonation system. The device is composed of a (1) jacketed tank, (2) peristaltic pump, (3) thermostatically controlled bath and (4) gas diffusor.

398x379mm (236 x 236 DPI)

Figure 2a.



Figure 2b.



Figure 3.









Figure 5a.







Figure 5c.



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 Table 1. Ozone decomposition. Kinetic parameters.

[O ₃] (g Nm ⁻³)	T (°C)	k _{pCBA} [•OH] (L mol ⁻¹ min ⁻¹)	r ²
21.15	20	0.0366	0.987
	40	0.0603	0.994
	50	0.0666	0.995
	60	0.0728	0.996
	20	0.0655	0.988
42.3	40	0.0942	0.993
	50	0.1145	0.992

T (°C)	[St] ₀ (mg L ⁻¹)	k_{St} [•OH] (L mol ⁻¹ min ⁻¹)	r ²	
40	600	34.6	0.991	
	1300	35.1	0.991	
	600	38.4	0.943	
50	1300	38.6	0.956	
	1700	38.9	0.938	
	600	42.2	0.891	
60	1300	41.6	0.955	
	1700	42.2	0.890	