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**Recommended Methods to Study Resistive Switching Devices**

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### Article

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### **Recommended methods to study resistive switching devices**

*Mario Lanza\*, H.-S. Philip Wong, Eric Pop, Daniele Ielmini, Dimitri Strukov, Brian C. Regan, Luca Larcher, Marco A. Villena, Jianghua J. Yang, Ludovic Goux, Attilio Belmonte, Yuchao Yang, Francesco M. Puglisi, Jinfeng Kang, Blanka Magyari-Köpe, Eilam Yalon, Anthony Kenyon, Mark Buckwell, Adnan Mehonic, Alexander Shluger, Haitong Li, Tuo-Hung Hou, Boris Hudec, Deji Akinwande, Ruijing Ge, Stefano Ambrogio, Juan B. Roldan, Enrique Miranda, Jordi Suñe, Kin Leong Pey, Xing Wu, Nagarajan Raghavan, Ernest Wu, Wei D. Lu, Gabriele Navarro, Weidong Zhang, Huaqiang Wu, Runwei Li, Alexander Holleitner, Ursula Wurstbauer, Max Lemme, Ming Liu, Shibing Long, Qi Liu, Hangbing Lv, Andrea Padovani, Paolo Pavan, Ilia Valov, Xu Jing, Tingting Han, Kaichen Zhu, Shaochuan Chen, Fei Hui, Yuanyuan Shi*

Prof. M. Lanza, Mr. X. Jing, Ms. F. Hui, Ms. Y. Shi, Mr. K. Zhu, Ms. T. Han, Mr. S. Chen

Institute of Functional Nano& Soft Materials (FUNSOM), Collaborative Innovation Center of Suzhou Nano Science & Technology, Soochow University 199 Ren-Ai Road, Suzhou, 215123, China. E-mail: mlanza@suda.edu.cn

Prof. H.-S. P. Wong, Prof. E. Pop, Dr. B. Magyari-Köpe, Dr. E. Yalon, Dr. M. A. Villena, Mr. H. Li

Department of Electrical Engineering, Stanford University, Stanford, California 94305 USA.

Prof. D. Ielmini

Dipartimento di Elettronica, Informazione e Bioingegneria, Politecnico di Milano and IU.NET, Piazza L. da Vinci 32, 20133 Milano, Italy.

Prof. D. Strukov

Electrical and Computer Engineering, University of California, Santa Barbara, CA 93106-9560, USA.

Prof. B. C. Regan

Department of Physics and Astronomy, University of California, Los Angeles, California 90095 USA.

Prof. L. Larcher

Dipartimento di Scienze e Metodi dell' Ingegneria, Università degli Studi di Modena e Reggio Emilia, Reggio, Emilia, Italy.

Prof. J. J. Yang

Department of Electrical and Computer Engineering, University of Massachusetts, Amherst, MA 01003, USA.

Dr. L. Goux, Dr. A. Belmonte

IMEC, Kapeldreef 75, B-3001 Leuven, Belgium

Prof. Y. Yang and Prof. J. Kang

Key Laboratory of Microelectronic Devices and Circuits, Institute of Microelectronics, Peking University, Beijing 100871, People's Republic of China.

Prof. F. M. Puglisi, Prof. P. Pavan

Dipartimento di Ingegneria "Enzo Ferrari", Università degli Studi di Modena e Reggio Emilia, Reggio, Emilia, Italy.

Prof. A. Kenyon, Prof. A. Mehonic, Dr. M. Buckwell  
Department of Electronic & Electrical Engineering, UCL, Torrington Place, London  
WC1E 7JE,  
United Kingdom.

Prof. A. Shluger  
Department of Physics and Astronomy, University College London, London WC1E  
6BT, UK

Prof. T. H. Hou, Dr. B. Hudec  
Department of Electronics Engineering and Institute of Electronics, National Chiao  
Tung University, Hsinchu 300, Taiwan, Republic of China.

Prof. A. Hou  
International SEMATECH, 2706 Montopolis Drive, Austin, TX 78741, U.S.A.

Prof. D. Akinwande, Ms. Ruijing Ge  
Microelectronics Research Center, The University of Texas at Austin, Austin, Texas  
78758, United States

Dr. S. Ambrogio and Dr. E. Wu  
IBM Research Division, 1000 River Road, Essex Junction, Vermont 05452-4299, USA.

Prof. Juan B. Roldan  
Departamento de Electrónica y Tecnología de Computadores, Universidad de Granada,  
Facultad de Ciencias, Avd. Fuentenueva s/n, 18071 Granada, Spain

Prof. J. Suñe, Prof. E. Miranda  
Departament d'Enginyeria Electrònica, Universitat Autònoma de Barcelona, Barcelona  
08193, Spain.

Prof. K. L. Pey and Prof. N. Raghavan  
Engineering Product Development Pillar, Singapore University of Technology and  
Design, 487372, Singapore.

Dr. X. Wu  
Shanghai Key Laboratory of Multidimensional Information Processing, Department of  
Electronic Engineering, East China Normal University, 500 Dongchuan Road, Shanghai  
200241, China

Prof. W. D. Lu  
Department of Electrical Engineering and Computer Science, University of Michigan,  
Ann Arbor, MI 48109 USA.

Dr. G. Navarro  
CEA-Laboratory of Electronics, Technology, and Instrumentation, Grenoble (LETI)  
Grenoble, Cedex 9, France.

Prof. W. Zhang  
Department of Electronics and Electrical Engineering, Liverpool John Moores  
University, Liverpool, L3 3AF, United Kingdom

Prof. H. Wu  
Institute of Microelectronics, Tsinghua University, Beijing 100084, China.

Prof. R. Li  
Key Laboratory of Magnetic Materials and Devices, Ningbo Institute of Materials  
Technology and Engineering, Chinese Academy of Sciences, Ningbo, Zhejiang, 315201,  
China.

Prof. Alexander Holleitner and Dr. Ursula Wurstbauer  
Walter Schottky Institute and Physics Department, Technical University of Munich,  
Germany

Prof. M. Lemme  
Chair of Electronic Devices, RWTH Aachen University, 52074 Aachen, Germany.

Prof. M. Liu, Prof. S. Long, Prof. Q. Liu, Prof. H. Lv  
Key Laboratory of Microelectronics Device & Integrated Technology, Institute of  
Microelectronics, Chinese Academy of Sciences, Beijing 100029, China.  
Dr. A. Padovani  
MDLab s.r.l., Via Sicilia 31, 42122, Reggio Emilia, Italy  
Dr. I. Valov  
Institut für Werkstoffe der Elektrotechnik 2, RWTH Aachen University, 52074 Aachen,  
Germany.

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## **Abstract**

Resistive switching (RS) is an interesting property shown by some materials systems that, especially during the last decade, has gained a lot of interest for the fabrication of electronic devices, being electronic non-volatile memories those that have received most attention. The presence and quality of the RS phenomenon in a materials system can be studied using different prototype cells, performing different experiments, displaying different figures of merit, and developing different computational analyses. Therefore, the real usefulness and impact of the findings presented in each study for the RS technology will be also different. In this manuscript we describe the most recommendable methodologies for the fabrication, characterization and simulation of RS devices, as well as the proper methods to display the data obtained. The idea is to help the scientific community to evaluate the real usefulness and impact of an RS study for the development of RS technology.

## 1. Introduction

Resistive switching (RS) is the property shown by some materials of cyclically changing their electrical resistivity between different stable resistance levels when exposed to specific electrical stresses [1]. This property is interesting because these resistive states can be used to represent different logic states (e.g. the ones and zeros of the binary code), which may be useful for many digital applications (e.g. detectors [2], information storage and computation [3-4]). Most studies on RS materials and devices (~95% [5]) reported stable RS between two resistive states, namely high resistive state (HRS) and low resistive state (LRS). Some materials and devices show the ability of achieving more than two stable resistive states [6], (in this case the nomenclature HRS and LRS is replaced by state 1, state 2, state 3, etc...), which may be used for multilevel information processing applications. However reliably distinguishing each conductive state in multilevel devices is much more challenging due to the intrinsic variability of the device parameters (currents, switching voltages) in each state (see section 3.4). This issue becomes extremely challenging when studying large group of samples statistically.

When fabricating a RS device the material showing the RS capability (namely RS medium, which is typically an insulator) is sandwiched between two electrodes (in most of reports vertically [7]), leading to a micro- or nanoscale metal/insulator/metal (MIM) cell —the metallic electrodes are integral parts of the devices, i.e. the RS medium alone does not completely determine their characteristics. RS devices using semiconducting electrodes, i.e. forming metal/insulator/semiconductor (MIS) structures, have been also reported [8, 9]. The first RS cells reported date from 1967 [10], and consisted on Au (30nm) on SiO<sub>2</sub> (300 nm) on Al junctions with a lateral device area of 9 mm<sup>2</sup>. Over time new materials combinations appeared, and currently RS can be

readily achieved in various RS media, including transition metal oxides (TMOs) [11-14], chalcogenides [15-16], polymers [17-18], and two-dimensional (2D) materials [7]. The most common pure metals used as electrode are Pt, Au, Ag, Ti, Ni and Cu [1,19], although TaN and TiN are preferred in the industry [20].

Different material combinations used in MIM cells require different types of electrical stresses in order to show RS, i.e. to induce HRS-to-LRS (set) and LRS-to-HRS (reset) transitions. Hence, the RS phenomenon can be classified into: *i*) unipolar and *ii*) bipolar RS, when the set and reset processes need to be triggered by applying stresses of the same or opposed polarity, respectively [1]; *iii*) non-polar RS, when the set and reset transitions can be achieved by applying stress of any polarity [21]; and *iv*) threshold RS, when the LRS is volatile and the reset process takes place automatically when the stress is switched off [22]. Moreover, depending on the space occupied by the atomic rearrangements responsible for the state change, RS phenomenon may be also classified into: *i*) filamentary and *ii*) area-dependent [1]. RS is called filamentary if the atomic rearrangements inducing the switching take place in the form of small (<100 nm<sup>2</sup>) spots within the RS medium. This mechanism is very similar to a reversible dielectric breakdown (BD) driven by the formation of one/few conductive filament/s (CF), and it is characterized by its fast switching speed (~300 ps) [23], high LRS/HRS current ratios (namely  $I_{LRS}/I_{HRS}$ , up to  $10^9$  [24]), and excellent integration capability ( $10^{11}$  bits/cm<sup>2</sup> [3]). However the high currents in LRS may increase the power consumption, plus the complexity of controlling the set/reset transition (due to their stochastic nature) results in a high cycle-to-cycle and cell-to-cell variability [25]. On the contrary, RS is called area-dependent if the RS is a homogeneous phenomenon that takes place at most of the locations laterally displaced (same depth) within the insulator. Area-dependent switching may happen at one or both metal/insulator interfaces, or even

at the central depth of the insulator, and is related to diffusion effects and interface phenomena [1, 26-27]. Distributed RS has the advantage of a lower power consumption (as no CF is completely formed/disrupted in each state transition the currents in LRS cannot be so high), but the  $I_{LRS}/I_{HRS}$  ratios and switching speeds are not as competitive as in filamentary RS devices. Phase change materials may be considered area dependent, as the atomic rearrangements take place in the entire volume of the RS medium. However, their performance is closer to filamentary materials, as the atomic rearrangements effectively connect both metallic electrodes. Therefore, phase change materials and devices deserve special attention due to their high performance (i.e. switching speed, endurance) and impact in the RS device community [28], and many of the fabrication and characterization methods discussed in this article are also applicable to them. The combination of layers with different properties is also a valid strategy to achieve specific performances. Recently RS cells using stacked bilayer RS media have shown both filamentary and distributed RS simultaneously [9] which may be useful to build up RS devices with combined capabilities.

RS-based electronic products can include different amounts of RS cells depending on their applications, ranging from few (<10) in detectors [2] and logic gates [29], to billions in non-volatile memories (NVM) [30] and artificial neural networks [31]. The main challenges in the fabrication of RS-based NVMs are to ensure that all devices show good performance (see Table 1), and that all the RS cells within the RS device show nearly identical RS behaviors (i.e. low cell-to-cell variability). In fact this second requirement is currently the greatest challenge (see section 3.4) [3, 25], and it is hindering the industrial mass production of RS-based NVMs. During the past decade the NVMs manufacturers have been the main players boosting RS technologies —this is a huge global market (47 billion United States Dollars in 2016 [32]) that is expected to

double by 2020 [33])—. Consequently, several NVM devices based on the RS phenomenon have been proposed during the past years, including the resistive random access memory (RRAM) and phase change memory (PCM) [25], and they have reached competitive performances compared to mainstream memories (i.e. static RAM, dynamic RAM, NOR and NAND Flash) and other emerging memories (i.e. Ferroelectric RAM, spin-transfer-torque magnetic RAM) [34-35].

RS-based NVMs started to be commercialized in 2015 by Panasonic [36] and Adesto [37] also placed some RS based products in the market. However, despite the great progress achieved, RS-based NVMs are still not sufficiently robust for mass information storage [25], and for this reason the devices commercially available are still restricted to very specific applications (*e.g.* controlling sensors [38]). Other RS applications, such as the use of RS cells as electronic synapses in artificial neural networks and neuromorphic computing [39] remain incipient, but their potential is greater, as they represent a completely new computing architecture with multiple applications (not only information storage). However, there is still no consensus on the performance metrics required of RS devices in order to be used as electronic synapses in artificial neural networks.

Research in RS devices is expected to be a very active field in the next decade, boosted by the Internet of Things [40], and strong efforts need to be put into developing reliable RS technologies. Unfortunately, in recent years different methodologies have been used to fabricate, characterize and simulate RS devices, being their real impact in RS technology and RS knowledge completely different. In this paper, we aim to clarify which are the correct methods for the study of RS devices, and how to provide useful knowledge for industrial RS technologies. This paper is focused on the fabrication and characterization of RS-based NVMs, as their performance and reliability criteria are the

highest among all RS applications, but the methods presented here may be also applied for any type of RS device. This paper contains three technical sections, device fabrication (section 2), device characterization (section 3), and device simulation (section 4), in which several technical recommendations are discussed, and a final section discussing the perspectives and challenges for the next years in RS science and technology (section 5).

## **2. Device fabrication**

The study of RS in different materials is normally conducted in one or few MIM cells (test structures), as most laboratories in universities and research institutes do not have the capability to fabricate an entire RS product. Three kinds of MIM test structures are the most common when studying RS: *i*) common bottom electrode (BE, **Figure 1a**), *ii*) cross-point (Figure 1b), and *iii*) cross-bar (Figure 1c). The first one uses a conductive substrate that serves as common BE for all the MIM cells [41]. Then, an insulating film is deposited on its entire surface and finally several top electrodes (TE) with a specific area can be patterned along the surface of the insulator [42]. A top-view scanning electron microscopy (SEM) image of matrices of RS cells (with different sizes) fabricated using this method is displayed in Figure 1a. Instead of a conductive substrate, an insulating substrate covered with a metallic film can be also used, but in that case the insulator should not cover the entire surface of the underlying metal film, which needs to be contacted for electrical characterization.

After fabrication, the devices can be characterized in a probe station connected to a semiconductor parameter analyzer (SPA) by contacting to the TE and BE. If very small TEs are fabricated, they might also be contacted using the probe tip of a

conductive atomic force microscope (CAFM) [43], although one needs to have in mind that: *i*) the tip/electrode contact may not be as good as in the probe station (e.g. molecules of water from the relative humidity of the environment may be present between the tip and the electrode), reducing the overall detected current [44], *ii*) the tip conductivity may degrade fast [45], *iii*) the electronics of standard CAFMs present important limitations for the measurement of RS [46] (see section 3.5), and *iv*) the measurement process is more complex, i.e. a topographic map is required to find the electrode on which the tip will be placed, and therefore the characterization time will be much longer. For these reasons, the use of CAFM to test MIM cells (placing the CAFM tip on the top electrode) has not widespread, and in RS research CAFM is mostly used for studying scalability [9], as well as to distinguish which locations of an insulator drive RS and which do not [47-48] (in both cases the CAFM tip serves as top electrode). Therefore, the main problem of the device structure in Figure 1a is that the minimum size of the devices that can be characterized with the tip of the probe station is always  $>100 \mu\text{m}^2$ .

To solve this problem, cross-point RS cells can be fabricated (see Figure 1b) [49], although their fabrication process is slightly more complex because it involves two lithography steps: deposition of the BE and TE, and ideally a third photolithography step to etch the RS medium deposited on the BE may be also necessary. In this case the metallic pads for probe station contact are still large (typically  $10^4 \mu\text{m}^2$ ), but the sandwiched MIM area can be much smaller. Using photolithography and electron beam lithography (EBL) cross-point MIM cells as small as  $1 \mu\text{m} \times 1 \mu\text{m}$  [50] and  $10 \text{ nm} \times 10 \text{ nm}$  [51] can be fabricated, respectively. While cross-point structures can be very competitive for RS studies in terms of scalability, some genuine circuit level factors (such as sneak path leakage currents [52]) cannot be analyzed using this kind of

structure. For such purpose, some reports built planar [53-54] and three-dimensional (3D) [55] cross-bar arrays (see Figure 1c). In this case the MIM cells are interconnected with thin wires that end up in large pads [53], so they can be characterized using the probe station. The test setup for advanced cross-bar circuit structures typically requires die packaging and dedicated printed circuit board or custom probe card in combination with switch matrix tool [56]. Note that the term cross-bar refers to a collection of interconnected cross-point devices; therefore, using the term cross-bar to refer to a single and isolated cross-point structure is misleading.

Thus, the types of structures used to characterize RS may vary a lot, and therefore the impact of the knowledge extracted from each of them will be also very different. The preferred configuration is the cross-bar because it is the most demanded for realistic RS products, although cross-point can also provide very accurate information about the functioning of one single RS cell. However, if the RS cells embedded in the cross-bar array don't have enough non-linearity, the signals collected when studying a specific cell may contain contributions from the adjacent ones. For this reason it is recommendable that studies on cross-bar RS structures also include data about isolated cross-point devices.

The most important parameter when studying RS devices is the area of the MIM cell —that affects the currents in HRS ( $I_{\text{HRS}}$ ), and sometimes also in LRS ( $I_{\text{LRS}}$ , e.g. in devices with distributed RS mechanism). In CF-based devices the RS is a stochastic process that always takes place at the weakest locations of the sample [57]; if the device size is larger the probability of finding weaker points is larger, which modifies the set and reset voltages ( $V_{\text{SET}}$  and  $V_{\text{RESET}}$ , respectively). This produces different BD energies that create CFs with different sizes, and subsequently the characteristics of the devices are also different. In general, smaller CF-based RS devices show lower  $I_{\text{HRS}}$  and larger

$V_{\text{SET}}/V_{\text{RESET}}$  [22]. For this reason vertical MIM structures with a common bottom electrode and large ( $>100 \mu\text{m}^2$ ) top electrodes should be avoided; when the fabrication of cross-bar and cross-point structures is impossible, vertical MIM structures with large electrodes should be combined with nanoscale electrical characterization experiments (e.g. CAFM, see section 3.5) in order to confirm good RS scalability [9], which is essential to demonstrate that the findings are applicable to ultra-scaled devices. Another disadvantage of devices made of a common BE with large TEs (as in Figure 1a) is that the tip of the probe station exerts a non-negligible pressure in the active area of the RS device, which may change the characteristics measured due to mechanical stress. Ideally, the area of the MIM device should be as small as possible. Refs. [58] and [59] reported MIM-like RS devices with diameters of 10 nm and 28 nm respectively (see Figure 1d).

Furthermore, the methods involved in the fabrication of the RS cells and devices (e.g. metal and RS medium deposition and lithography) are critical for ensuring the good quality of the results. In particular, minimizing thickness fluctuations and maintaining clean interfaces (between the metallic contacts and the RS medium) is mandatory. Keeping the vacuum between each step is also beneficial for the RS devices, although in many cases that may not be possible because the electrodes and RS medium might be fabricated using different equipments. In the following sub-sections some specific technical advice for each process step is given.

## **2.1. Selecting the bottom electrode**

The surface of the substrate used needs to be as flat as possible, as that would reduce the number of bonding defects and avoid thickness fluctuations of the layers deposited on top; this is critical to reduce cell-to-cell variability. The best way is using a

Si wafer covered by a few-hundred nanometer  $\text{SiO}_2$  film as substrate; the reason is that such substrate has a root mean square (RMS) surface roughness  $<0.2$  nm [60], which is similar to the roughness of industrial wafers on which real RS devices should be integrated. The  $\text{SiO}_2/\text{Si}$  wafer should be covered with a metallic film as BE (the recommended thickness is  $>50$  nm to withstand the high current densities in LRS). This metallic film may cover the entire surface of the  $\text{SiO}_2/\text{Si}$  wafer if working with RS cells that share a common BE (see Figure 1a), or just cover some specific areas to delimitate cross-point or cross-bar bottom electrodes (see Figures 1b and 1c). The use of noble metals (Au, Pt) as BE is more common than metals that can easily oxidize (Ti, Cu) — and recommendable when working in university labs without exhaustive air and humidity control— because they collect less oxygen from the atmosphere during the time between bottom electrode and RS medium deposition (although in the industry noble metals may not be used due to their high cost and etching issue). It should be noted that introducing oxygen intentionally in the RS devices is fine but in a controllable way, e.g. using thermal treatments or doping techniques; the adsorption of oxygen from the atmosphere to form RS media [61] is always undesired. However, the adhesion of Au or Pt to the surface of the substrate ( $\text{SiO}_2/\text{Si}$  wafer) may be not ideal, and sometimes an interfacial film of few-nanometers Ti may be used to facilitate its adhesion [62]. It should be noted that (ultimately) the use of industry-compatible conductive alloys (TaN, TiN) is desired, although controlling the amount of oxygen may be challenging in laboratories of several universities and research institutes (in such case, using noble metals may lead to better quality interfaces). For metal deposition the use of electron beam evaporation (EBE) is the most recommended tool because it leads to a very smooth surface, although sputtering also leads to an acceptable surface

roughness. The worst option for metallic substrate (bottom electrode) is the use of metallic foils [63], as their surface can be very rough (RMS > 100 nm) [64].

## **2.2. Deposition of the RS medium**

The deposition of the insulating film is the most critical step, and its surface needs to be as smooth as possible to avoid cell-to-cell variability. The most common techniques used for TMO deposition are atomic layer deposition (ALD) [65] and sputtering [66]. While the use of ALD can lead to surfaces as smooth as RMS <0.2 nm [67], the surface roughness of sputtered films (RMS <1 nm [68]) is still acceptable for RS applications. In fact, in some cases sputtered RS media have shown better RS performance than ALD ones (i.e. as-grown ALD HfO<sub>2</sub> does not show RS [47] while sputtered HfO<sub>2</sub> does [69]) due to their larger initial density of defects, which can trigger the initial BD at lower voltages, producing less damage in the insulator and preventing irreversible BD [47]). Moreover, stoichiometry control is more straight forward in sputtering than ALD. However, it should be noted that in 3D cross-bar devices the RS medium must be deposited in the vertical sidewalls of high-aspect-ratio holes, and the only technique able to do this is ALD [70-74]. Many recent reports showed several-layer 3D vertical RS devices where the RS films were prepared by physical vapor deposition; this may be good as a proof-of-concept, but these devices are not expected to show high performances in terms of cell-to-cell variability unless they are fabricated using ALD.

Several studies of polymers [17-18] and 2D materials [7, 74] as RS medium used the spin coating technique: a drop of liquid-phase material is deposited on the substrate (common BE) and spun (at 1000-3000 rpm for 1-3 minutes, depending on the

viscosity of the material used); afterwards the sample is normally heated at moderate temperatures (below 100 °C) for a few (<5) minutes. This process leads to the formation of a film with thicknesses always >100 nm [74], and a surface roughness much larger than that of TMO-based RS cells, i.e. RMS >10 nm [74]. When using the spin coating methodology the risk of prohibitive cell-to-cell variability is very high due to the large surface roughness (if the surface of the BE is very flat and the RS medium surface is very rough, that would produce thickness fluctuations from one device to another). In recent years several publications fabricating RS cells via spin coating of novel 2D materials [7, 74], polymers [17-18] and chalcogenides [15-16] appeared, and they demonstrated a proof-of-concept observation of RS through one/few cycles. Unfortunately, none of them included cell-to-cell variability information, and in most cases even the total number of devices characterized was not indicated. In fact we are not aware of any work using spin coating technique combined with cross-point structures, meaning that all known studies apply to large device sizes >100  $\mu\text{m}^2$ ; therefore, additional corroborations of those findings in smaller RS cells are necessary.

It should be highlighted that, independently of the deposition method, when depositing the RS medium on metal-coated  $\text{SiO}_2/\text{Si}$  wafers it is recommendable to keep a part of the BE exposed, so that it can be later contacted with the tip of the probe station. Several groups do not follow this step and later scratch the surface of the insulator with the tip of the probe station (applying a vertical/lateral mechanical stress using the screws of the tip manipulator). Although this method works, it should be avoided when possible because it may damage the probe station tips and reduce the lifetime of the devices (e.g. if the thickness of the bottom metal is reduced due to scratching, it may be more susceptible to melting due to high currents during LRS, which may reduce the endurance of the RS cells).

### 2.3. Patterning the top electrodes

When working with cross-point and cross-bar structures, the electrodes (both BE and TE) are deposited via photolithography or EBL combined with metal deposition (e.g. EBE or sputtering). The use of lithographic techniques ensures that all test structures will have the same shape, and avoids the deposition of metal outside the selected areas (i.e. no metal can penetrate below the photoresist). The only drawback is that the surface of the RS medium needs to be initially covered with a film of photoresist that is later removed, and that may lead to polymer residue contamination [75] (see **Figures 2a** and **2b**). Although the developing process of the photoresist could be improved and the samples might be intensively cleaned, one should note that the surface of a material as-deposited will be always cleaner than after exposure to photoresist and developing, especially if this process is not done in the industry.

When working with devices that use a common BE (see Figure 1a), this problem can be mitigated by using a shadow mask, which also eases the entire process. A shadow mask is simply a piece of metal with holes patterned exactly with the shape of the electrodes to be deposited, and it is placed directly on the sample during metal deposition. However, the use of shadow masks may bring other undesired problems, such as deviation on the shape and size of the holes (Figure 2c), and penetration of metal below the mask (i.e. out of the areas reserved for the electrodes, see Figures 2e-h). Nevertheless, if a laser-patterned shadow mask is used (see Figure 2d) these problems can be minimized [62]. Some studies used the metallic grids for specimen holder in transmission electron microscopy (TEM) as shadow mask [76]; while this is a clever and cheap way to pattern electrodes with well-defined shapes, it needs to be said that the

typical size of the holes in a TEM grid is too large ( $\sim 300\ \mu\text{m}$  in diameter), and only one size per sample is available. We note that (for the same lateral size) electrodes patterned on flat surfaces using a shadow mask can be more easily distinguished and contacted in the probe station than those patterned on rough surfaces. We are aware of some studies patterning top electrodes using a shadow mask and silver paint (spread using a brush) [63]. It should be emphasized that this process leads to a bad interface and should be avoided by all means.

#### **2.4. Fabrication RS cells based on 2D materials**

When fabricating RS devices using 2D materials additional challenges exist, depending on the process used to synthesize the 2D material. The best quality material is normally achieved by mechanical exfoliation, but this leads to small material flakes (typically  $<10\ \mu\text{m}$ ) with uncontrollable thicknesses [77], and it requires EBL to pattern the electrodes [78]. This makes it very difficult (if not impossible) to collect statistical information. The two most widespread methods to synthesize 2D materials applied to RS devices are chemical vapor deposition (CVD) and liquid-phase exfoliation [7].

CVD can be used to grow high quality graphene [79], molybdenum disulfide ( $\text{MoS}_2$ ) [80], molybdenum diselenide ( $\text{MoSe}_2$ ) [81], tungsten disulfide ( $\text{WS}_2$ ) [82], tungsten selenide ( $\text{WSe}$ ) [83], and hexagonal boron nitride ( $h\text{-BN}$ ) [84-86], among many others. The problem is that the temperature used for the growth is typically  $>700\ \text{°C}$ , which prevents growing the 2D material on wafers with existing integrated circuits due to diffusion problems; the maximum temperature allowed for complementary metal-oxide-semiconductor (CMOS) back-end of line integration is typically  $450\ \text{°C}$  [87]. Recently, thermally assisted conversion of metallic films at

CMOS back-end compatible temperatures has been demonstrated to yield promising layered films, such as platinum diselenide (PtSe<sub>2</sub>) [88-90]. A solution commonly employed is to synthesize the 2D material on the most suitable substrates (metallic foils for graphene [79] and *h*-BN [84-86] and SiO<sub>2</sub> or sapphire for 2D transition metal dichalcogenides (TMDs) [80-82]) and transfer it on the desired sample using different methods [91-93], being the wet transfer with the assistance of a polymer scaffold the most used by the RS community [93]. However, three main issues need to be taken into account: *i*) if the 2D layered material is too thin (e.g. monolayer) and the top electrodes are very large ( $>10^4 \mu\text{m}^2$ ) [94], the 2D material below the TE is likely to contain cracks (see **Figure 3a**). This is not a problem of a researcher doing a wrong transfer, as transferring monolayer 2D materials at wafer scale without producing cracks is (unfortunately) not possible using the current transferring technologies. This is a problem because at those locations with cracks the vertical structure will be less resistive, and CFs will always form there. In fact, the presence of holes and pores in 2D materials has been used to control the location of CFs [95-97]. Therefore, the currents may be flowing across a region without 2D material, and the knowledge extracted may not be applicable to the desired material structure. Nevertheless, if the device size is reduced to  $<25 \mu\text{m}^2$  this problem could be avoided (the density of cracks is not that high). In fact atomically thin RS devices with high  $I_{\text{LRS}}/I_{\text{HRS}}$  ratios  $>10^4$  could be fabricated using several different types of monolayer materials, including *h*-BN and 2D TMDs (of the form MX<sub>2</sub>, where M=Mo or W, and X = S or Se) [98]. As far as the switching mechanism is concerned, on one hand a filamentary model was proposed based on area-dependent studies [98], and on the other hand local laser annealing showed that the work function of MoS<sub>2</sub>/Ti contacts can be intentionally tuned, leading to a distributed change on the resistivity [99]. Despite these two works are not in

conflict, more studies analyzing single layer RS media are necessary. Another way of avoiding the generation of cracks in the 2D material during its manipulation is to use thicker 2D layered stacks, which may be also useful to increase the current  $I_{LRS}/I_{HRS}$  in the RS device [62, 100]. *ii)* the transferred 2D material may contain some wrinkles and polymer residue. While wrinkle- and polymer-free 2D materials are preferred, it should be noted that such locations are more resistive, meaning that the CFs will not form there when the electrical field is applied (see Figure 3d). Therefore, the presence of wrinkles and polymer residue in RS devices based on 2D materials can be understood as a reduction of the effective area of the device [101]. It should be also noted that one method to avoid the formation of wrinkles in 2D materials is to enhance the roughness of the substrate where it is transferred [102]. And the third issue is *iii)* the transferred 2D material may contain several metallic impurities, e.g. from the metallic substrate where it was grown [103] or mobile ions originating from the environment [104]. In Ref. [103] it was demonstrated that present transfer techniques could lead to metallic residue concentrations exceeding  $10^{13}$  atoms/cm<sup>2</sup>, when the maximums allowed by the CMOS industry are below  $10^{10}$  atoms/cm<sup>2</sup> [105].

Unfortunately, the CVD growth of graphene and *h*-BN on metal-coated wafers is still very challenging due to metal de-wetting at high (>800 °C) temperatures. Ref. [106] achieved the growth of *h*-BN via CVD on metal-coated wafers, but only *h*-BN stacks were characterized and no device was fabricated. Some studies tried to reduce the growth temperature of 2D materials, but that leads to much lower quality (which may not be necessarily bad for the fabrication of RS media). More studies in this direction are necessary.

Two additional remarks when working with CVD-grown 2D materials are: first, it is important that the layered structure is confirmed [7], otherwise the devices may not

show the genuine behaviors of these materials —especially important for RS devices is the high thermal conductivity of 2D layered materials—. In fact, we are aware of some studies claiming the use of layered graphene and *h*-BN when the cross sectional TEM images reveal clear amorphous structure [107-108]. And second, RS devices using planar (lateral) graphene [109-110] and MoS<sub>2</sub> [111] structures have been reported; however, these structures are not sufficiently compact for realistic applications, and the mechanisms (electromigration, grain boundaries modification) cannot be controlled accurately. For these reasons, planar resistive switching configurations have not raised the interest of the industry.

When the 2D materials are assembled by liquid-phase exfoliation, the main concern is the same as when using other spin coated materials: process and roughness induced variability (see section 2.3). For this reason, in RS studies using spin-coated 2D materials, it is extremely important to include variability information.

### **3. Device characterization**

When studying the RS performance of MIM cells the way in which the electrical characteristics are collected is critical for making a correct interpretation. Normally the electrical tests are carried out in a probe station, and the most common figure of merit is the collection of two current vs. voltage (I-V) sweeps: one showing the set and another showing the reset process (see **Figure 4**). To do so, one of the electrodes in the MIM cell is grounded, and a ramped voltage stress (RVS) is applied to the other one [1]. In most cases the use of a current limitation is necessary in order to limit the energy delivered (and damage introduced) during the BD, otherwise the stress may lead to an irreversible BD and no reset would be detected in subsequent I-V sweeps [1]. However,

this observation (proof-of-concept) is not sufficient for understanding the nature and quality of the RS phenomenon in a MIM cell, and several other figures of merit including endurance, data retention, switching time, power consumption, variability, scalability and charge transport mechanism must be studied as well. In addition, it is important to note that I-V sweeps do not match the operating conditions of realistic devices, which work under short (<100 ns) pulsed voltage stresses (PVS) [1]. In the following subsections all these figures of merit and the most suitable methods to acquire them are discussed in detail.

### 3.1. Endurance

In a RS device endurance is defined as the number of times it can be switched between two (or more) resistive states keeping enough resistance ratio between them [3, 7]. Therefore, an endurance test consists of finding out what is the maximum number of set/reset transitions (cycles) for which RS phenomenon with enough current on/off ratio can be measured, and its common figure of merit is the  $R_{HRS}$  and  $R_{LRS}$  vs. cycle (see **Figure 5**). The failure of the device may not happen in one specific cycle, but it may be progressive [112]. Therefore, one needs to set up a threshold current on/off ratio below which the device is considered to have failed. However, the criterion to define RS device failure may be different depending on the application. In Ref. [113] the authors defined an  $I_{ON}/I_{OFF}$  ratio of 5 for considering device failure. While this may be perfectly fine for their application, other authors may consider it inadequate for other cases.

The endurance characteristics of RS cells can be obtained by performing different experiments, three of them being the most common: *i*) I-V sweeps, *ii*) current-visible PVS, and *iii*) current-blind PVS. The first experiment consists of the collection

of sequences of I-V sweeps in a single RS cell (like those in Figure 4), and the subsequent extraction of  $R_{HRS}$  and  $R_{LRS}$  dividing a selected read voltage (typically  $\pm 0.1V$  [9]) by the corresponding currents observed in the I-V sweeps at that voltage (see Figure 5a). This method is reliable because one can ensure the correct switching of the device in each cycle. A challenge is that this method is very slow, because the time required for collecting an I-V sweep can be very long ( $\sim 30-60s$ ), especially if low currents ( $< 1nA$ ) are measured. Moreover, the I-V sweep method does not match the stresses applied to realistic devices (they operate via PVS), and therefore the data presented using this method may not be strictly representative of the endurance of the same RS cell under real operation conditions.

The second experiment consists of the application of a train of PVS, in which the user can modify the voltages ( $V_{UP}$  and  $V_{DOWN}$ ) and times ( $t_{UP}$  and  $t_{DOWN}$ ), and simultaneously measure the currents driven [114] (namely current-visible PVS method). Normally one pulse with large  $V_{UP}$  ( $|V| > 1V$ ) is used to set/reset the devices, and read pulses are intercalated to read the conductance of the RS cell after each stress ( $V_{READ} = 0.1V$ ). Then, the values of  $R_{HRS}$  and  $R_{LRS}$  can be calculated for all test cycles (as in the I-V sweeps method, see Figure 5b). The current-visible PVS method is much faster than the I-V sweeps because the pulse widths can be of the order of microseconds, which allows collecting millions of cycles in few minutes; moreover, this method matches well the functioning of realistic devices. A challenge is that the PVS method often requires advanced hardware; for example, the Keithley 4200 SPA (equipment commonly used by many groups for these tests) requires an additional module to do this experiment, which involves additional cost.

The third experiment consists of the application of PVS but without measuring the current simultaneously (namely current-blind PVS). After a specific number of PVS

cycles without measuring the current, the stress is stopped and the resistivity of the RS cell is measured in DC mode or collecting an I-V sweep. This method does not require advanced hardware, all commercial SPA (and even pulse generators) can do this experiment, and it as fast as the normal PVS that measures the current in each cycle. The endurance characteristics collected using this method can be clearly distinguished because the data points are very spaced [13] (see Figure 5c). However, unlike the I-V sweep and PVS methods, the current-blind PVS method cannot ensure that 100% of the pulses applied actually induced state transitions in each cycle. E.g. Ref. [13] claims RS during more than  $10^6$  cycles, but only 24 data points for each resistive state are displayed; the same happens for Ref. [115], in which an endurance of  $10^7$  cycles is claimed, but only 70 data points are displayed. Actually, Refs. [13] and [115] did not explain if they measured the current during each cycle, but we assume that they used current-blind PVS due to the low amount of data points displayed—if one measures the current in each cycle and has the data, surely he/she will display them, as the authors in Ref. [114] did (see Figure 5b)—. For this reason the current-blind PVS method should only be used in very well optimized technologies at the industrial stage, and scientists based in universities and research institutes should avoid the use of this method to characterize the endurance of their prototypes. It is important to understand that using current-blind PVS to evaluate the endurance of incipient RS cells (such as RS cells based on 2D materials [115]) is not a reliable choice, as that can easily produce endurance overestimation; therefore the endurance values reported in such kind of studies (e.g. Refs. [13] and [115], although there are many others) should be further corroborated using the normal PVS method (i.e. measuring the current in each cycle).

Another issue that may affect the endurance of the cells is the relaxation time during the I-V curves or pulses. Normally the larger the relaxation time, the higher the

endurance measured. Therefore, it might be possible that endurance tests using I-V curves and current-blind PVS may result on higher endurance than the normal PSV method. Some works have applied triangular or sinusoidal signals (no relaxation time) to switch RS devices [116-117], but to the best of our knowledge this method has been only used for proof of concept switching, not for endurance tests. It should be highlighted that when measuring extreme endurance up to  $10^{12}$  cycles even current-visible PVS method could still be too slow. For example, considering that monitoring one entire RS cycle via current-visible PVS method takes  $\sim 1$  ms (including the duration of the first read pulse, set pulse, second read pulse and reset pulse, plus the time distance between them), the time required to measure endurance of  $10^9$ ,  $10^{10}$  and  $10^{11}$  cycles would be 11.5, 115 and 1157 days (respectively). An acceptable method to characterize extreme endurance is to monitor the switching of each cycle during the first  $10^6$ - $10^7$  cycles using current-visible PVS method, and then shift to PVS-blind method (collecting a decent amount of  $\sim 50$  points per decade). Reducing a bit the time of the read, set and reset pulses is recommendable when measuring extreme endurance.

Currently, RS devices with an endurance up to  $10^{12}$  cycles have been reported in different types of MIM cells, including Pt/Ta<sub>2</sub>O<sub>5-x</sub>/TaO<sub>2-x</sub>/Pt [118] and Ta/TaO<sub>x</sub>/TiO<sub>2</sub>/Ti [119]. In this sense, there is consensus that tantalum oxides seem to be the RS medium providing the best endurance.

### **3.2. State retention**

Studying data retention of a non-volatile RS device consists of checking if the LRS and HRS are stable over time after the set and reset transitions (respectively) [3, 7]. To do so, after inducing the set/reset transition (either by an I-V sweep or a PVS) the state retention can be studied by applying a constant voltage stress (CVS) over time

using a low ( $\sim 0.1$  V) read voltage, and subsequently measuring a current vs. time (I-t) curve for each resistive state [22]. Therefore, the figure of merit for state retention analysis is the I-t curve, which is normally accompanied by the voltage used during the read I-t curve (often indicated either inside the plot or in the figure caption, see **Figure 6a**). Normally the challenging point is to keep a long retention time in LRS, as the atomic rearrangements introduced during the set stress may vanish over the time. On the contrary, in HRS normally the retention is not a concern because that is normally the natural state of the device, and if no or low bias is applied the device should remain in its. It should be noted that in most RS devices the retention in LRS strongly depends on the current limitation (CL) used during the set transition [22]. For example, in CF based RS devices a larger CL during the set I-V sweep produces a larger CF that is more stable over the time [120-121], which will enlarge the state retention time detected in the subsequent I-t curve [22]. Therefore, in order to correctly evaluate the retention time detected in LRS (and compare among different works), the CL used during the set process (I-V sweep or PVS) should be indicated next to the I-t plot.

The desired data retention for RS-based NVM technologies is 10 years at 85 °C [3, 7]. Obviously, state retention tests of 10 years are not doable, and for this reason normally much shorter times of few hours or days are reported [122-123]. We are aware of some reports that measured retention of few hours or days, and projected trends up to 10 years [124-125]. Doing consistent reliability projections of specific parameters of electronic devices is acceptable; for example, the time-dependent dielectric breakdown (TDDB) of gate insulators is normally projected over years, and this assumption is based on data obtained from stresses at voltages much larger than in real operation conditions [126]. However, several reports in the field of RS do not conduct any aggressive stress that allows doing such extrapolation. Therefore, such extrapolation is

not accurate and should be avoided. One correct methodology to evaluate the retention of RS devices in aggressive conditions is to increase the temperature during the CVS applied to obtain the I-t curve [127]. At high temperatures the atoms in the MIM cell acquire energy, which facilitates atomic rearrangements [128]; therefore, the retention measured in LRS at room temperatures will always be larger than that measured at higher temperatures. If this method is used, the temperature applied during the I-t curve measured to characterize the endurance should be indicated (as well as the read voltage). Actually, the best would be to measure the retention at several (preferably elevated, >80 °C) temperatures and extrapolating such data points, given any failures were observed [129] (see Figure 6b). Moreover, in several MIM cells the retention failure (i.e. the unwanted transition from LRS to HRS) occurs suddenly [130], meaning that elaborating predictions based on short-times I-t curves may be a bit risky. A projected endurance of 10 years has been reported based on I-t curves collected at 85 °C in Pt/TaOx/Pt [127] and Pt/Al<sub>2</sub>O<sub>3</sub>/HfO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>/TiN/Si [131].

It should be noted that threshold-type RS devices are those in which the RS is volatile, i.e. the retention time ranges from some microseconds to few seconds. Studying the retention time of threshold-type RS devices is interesting in the field of neuromorphic computing, as they are suitable to emulate short-term plasticity learning rules because the retention time of the RS cell can be also interpreted as the relaxation time of an electronic synapse [22]. If the relaxation of the BD takes place in seconds or faster (down to microseconds), measuring an I-t curve after the set stress (I-V sweep or PVS) may produce important information loss, as some non-negligible time passes between the end of the set stress and the read I-t curve. In this case, the recommended methodology to detect the relaxation of the BD event is to apply one or few PVS (to set the device) and keep measuring the current (at 0 V [132] or 0.1 V [22]) after it. As the

current measurement is not interrupted after the stress, the real relaxation process of the threshold device can be accurately studied (see Figure 6c). Unfortunately, most reports studying relaxation time of electronic synapses didn't include information about the variability of the relaxation time. In Ref. [133] the authors measured the relaxation time of Ti/h-BN/Au threshold-type RS devices during more than 500 cycles, and the variability of the relaxation time observed was strikingly low (<10%, see Figure 6d).

### 3.3. Switching time and energy consumption

Studying the switching time and energy consumption (per state transition) in RS devices require the application of PVS to the RS devices. Due to the positive feedback of the filament formation on the current, the forming and set transitions of RS devices are not self-limited. Therefore, careful electrical switching characterization requires a current limiting element in the circuit [134]. To limit parasitic capacitance effects during transient, it is required that this element is integrated *in situ* close to the RS device [135-137]. A transistor is commonly used for this in the well-known 1-Transistor/1-Resistor (1T1R) structure [136-137]. However, due to the strong non-linearity of the current versus source-drain voltage, it is far more convenient to use an integrated load resistor as current limiter (in a so-called 2R structure) if we aim at extracting the actual voltage dropped on the resistive element ( $V_{RS.DEV}$ ) during switching [138]. This applies particularly to the characterization of the power consumption of a resistive device.

In this respect, an appropriate setup would include a fast pulse generator, allowing to apply square or triangular pulses to one electrode of the 2R device structure, and a high-bandwidth oscilloscope, allowing to simultaneously acquire both the applied voltage and the transient current (see **Figure 7**) [138]. The applied voltage is acquired

on one channel of the oscilloscope connected to the TE, while the current is read-out by connecting the BE in series to the 50-ohm impedance-matched input resistance of the oscilloscope and converting into current the voltage generated on this shunt resistor—it is important to consider the shunt resistance and parasitic capacitance of the instruments used for electrical characterization, especially when using additional elements (e.g. transistor, resistor). Waveforms of both channels are then numerically processed to remove residual offset and noise. In this setup, the use of the 2R structure allows to calculate at any time the actual voltage  $V_{RS.DEV}$  dropping on the resistive device [138]. In order to also extract the  $V_{SET}$  and  $V_{RESET}$  it is convenient to apply triangular voltage ramps (see inset in Figure 7). The switching energy may then be calculated by integrating the current and voltage traces over time on the oscilloscope.

Using this methodology, the switching energy may be characterized for different operating currents by means of load resistors with various resistance magnitudes. On the other hand, minimum switching energies may be characterized by applying short pulses with high ramp rates [3-7]. Typically the switching transient is of the order of a nanosecond, and the required switching time for stable filament set and reset lies in the range of a few nanoseconds [136-137]. For a set experiment, we observe that after the set transition voltage snapback,  $V_{RS.DEV}$  stabilizes at a constant voltage during the transient ( $V_{TRANS}$ ).  $V_{TRANS}$  is an intrinsic parameter for a given resistor; it was observed to depend neither on the operating current nor on geometrical factors [138]. Moreover,  $V_{TRANS}$  varies only slightly in the range 0.4-0.7 V for a wide range of oxide-based resistive devices [137-139]. This means that the transient energy may be fairly approximated by multiplying the transient current by  $\sim 0.5$  V. Hence, for an operating current of 100  $\mu$ A, typical set energy and power lie in the range of  $\sim 1$  pJ and 50  $\mu$ W respectively. For the reset transition, it was observed that the maximum reset current is

similar to the maximum set current, while the reset voltage equals  $V_{\text{TRANS}}$ , meaning that the reset energy is similar to the set energy [138]. Note that this is a general but not systematic observation. For example, conductive bridge devices typically deviate from this behavior and exhibit different set and reset energies [140].

### 3.4. Variability

The spatial (cell-to-cell) and temporal (cycle-to-cycle) variation of the electrical characteristics (*i.e.*  $V_{\text{SET}}$ ,  $V_{\text{RESET}}$ ,  $I_{\text{HRS}}$ ,  $I_{\text{LRS}}$ ) of RS devices is still by far the most challenging obstacle towards widespread deployment of such devices in memory and computing applications. However, it is true that variability may be exploited for the development of useful systems, such as true random number generators, and physical unclonable function devices for security applications. In the field of neuromorphic computing the effect of variability is still under debate. Ref. [141] suggested that variability may be useful for stochastic computing, although this work used a threshold device. More works in this direction are necessary. Nevertheless, cell-to-cell and cycle-to-cycle variability is a major problem to be avoided in RS devices for information storage.

The main problem of the literature available in the field of RS is the lack of statistics often generates misleading information about the quality and stability of the memory window, leading to an excessively optimistic estimation of device performance. While cell-to-cell variability is something that could be solved by improving the fabrication process (*i.e.* providing homogeneous interfaces, identical sizes) the observation of large cycle-to-cycle variability is intrinsic in the physics of the device, and therefore influenced by the electrical stresses applied. The formation and rupture of

a CF is a stochastic process, and for that reason predicting and controlling the shape of the CFs (which is the key factor defining the electrical properties of the RS devices) is extremely challenging. For this reason, all RS studies should include information about variability and yield. Even when the authors show such information, comparisons are difficult because variability studies in RS devices may differ a lot from one group to another, as there is no consensus on a typical figure of merit, nor standard variability limits established by the industry [3, 7]. Here we propose the figures of merit indicated in **Figure 8** as a method to evaluate variability in RS devices.

In the case of cycle-to-cycle variability the endurance plot may be useful to understand how  $I_{HRS}$  and  $I_{LRS}$  change from one cycle to another (see Figure 5), but that gives no information on  $V_{SET}$  and  $V_{RESET}$ . A good example of cycle-to-cycle variability characterization is reported in Ref. [142], where several cycles were visualized (see Figures 8a and 8b). Recommended methods for studying the variability of the switching voltages and resistances are to plot the histogram (Figure 8c) or cumulative probability plot (Figure 8d) of each parameter. This allows to easily evaluate their value and deviation, which is very valuable information when designing the threshold level to distinguish both HRS and LRS. Figure 8d offers a clear example of the reduction of the memory window when large statistics are considered. The graph clearly shows that, while the median window is  $\sim 100\times$ , no window is present between the tails of the two distributions. When analyzing cell-to-cell variability, one good method is to measure several cells and highlight the median characteristic (see Figure 8e) [143]. However, in Figure 8e the information about the cycle-to-cycle variability is masked. In order to solve this problem, here we suggest some additional characteristics. One is to analyze  $V_{SET}$  and  $V_{RESET}$  variability by showing the cumulative probability plot of these parameters for each device superimposed (see Figure 8f). This plot is interesting

because it allows fast visualization of the variability within one single device and from one device to another. When analyzing the cell-to-cell variability of  $R_{HRS}$  and  $R_{LRS}$  one option may be showing an endurance plot with the data corresponding to several devices superimposed (as in Figure 8g), or showing the median characteristics together with an error bar for each data point, where the bar size represents the interval (as done in Ref. [144]). The latter enables to have a visual estimation of the cell-to-cell variability without crowding the plot with an excessive number of traces. Another possibility is to measure several (>100) I-V sweeps for different devices and plot together their median I-V sweep (see Figure 8h).

Switching variability has a strongly detrimental effect on the multilevel operation, which was initially considered one of the main advantages of RS technologies. The multilevel capability has been reported for a large plethora of RS devices, mainly thanks to the analog dependence of  $R_{LRS}$  ( $R_{HRS}$ ) on the  $I_{SET}$  ( $I_{RESET}$ ). Programming algorithms like incremental step pulse programming [145-147] and closed-loop pulse switching [59, 148] have allowed a better control of the multilevel operation in RS devices. However, in the vast majority of cases, the multilevel operation is reported either on single devices or for median resistance levels. When large cycle-to-cycle and cell-to-cell statistics are considered, the distinction between the distribution tails of adjacent levels (bits) fades, strongly frustrating the multilevel operation. The deleterious effect of variability on the multilevel operation can be tackled from different perspectives. For the cycle-to-cycle (intrinsic) variability, which is related to the stochastic nature of the resistive switching mechanisms, program or verify algorithms can be implemented in the external circuitry to set two resistance boundaries for each level of operation. This increases the design complexity and the total write time. On the other hand, cell-to-cell variability, which is process-related, can

be improved by aiming at a better uniformity across the wafer for the different integration steps. However, even when the programming variability can be strongly limited with the abovementioned solutions, the temporal variability hinders the multilevel operation. As reported in [149], even when program or verify algorithms are used to force the resistance below or above certain levels, the spontaneous rearrangement of the defects leads to an unpredictable drift of the resistive state. Considering all the effects reported in this paragraph, the multilevel operation is nowadays considered extremely challenging to implement in RS devices.

### **3.5. Scalability**

This is probably one of the most critical points in RS technologies and research. Researchers frequently report the RS behavior measured (via probe station) in devices with very large areas, of the order of  $100\ \mu\text{m} \times 100\ \mu\text{m}$  [63, 74], with a characteristic structure like that shown in Figure 1a (common BE). However, observations made in these devices may not be applicable to nanoscale devices, because the BD and RS are stochastic processes that take place at the weakest location in the total volume covered by the RS medium; statistically, larger devices (areas  $>25\ \mu\text{m}^2$ ) will show characteristics closer to those of dielectrically weaker locations, while real nanoscale devices (areas  $<100\ \text{nm}^2$ ) will show characteristics closer to dielectrically stronger locations. As an example, it has been demonstrated that smaller device areas lead to higher forming voltages [58, 22]. Different forming voltages generate CFs with different sizes across the RS device, which strongly affects its characteristics and lifetime.

For these reasons, it is always highly recommended to report the characteristics of RS devices for different device areas. The most recommendable is to go down to the nanoscale range, although that may be complex because the standard photolithography tools used in most universities and research institutes can only pattern devices with minimum lateral sizes of few micrometers ( $\sim 3 \mu\text{m}$ ). One option to pattern smaller devices is the use of EBL [51], but that may be more time consuming. In addition, the percentage of devices successfully fabricated (yield) via EBL is normally lower, as the removal of the polymer mask after metal deposition (lift-off process) may damage or detach the patterned metallic electrodes. Nanometer-scale RS devices have also been obtained using carbon nanotubes as the bottom electrode [150], or at the cross-point of two single-wall carbon nanotubes [151]. The latter cell areas are of the order of  $1 \text{ nm}^2$  (limited only by the small nanotube diameter) and they represent the ultimate lower limit of RS cell dimensions. Their drawback is the difficulty in fabrication, and to date only individual devices [150-151] but no device arrays could be fabricated with this approach.

Another option is the use of local characterization tools, such as scanning tunneling microscopy (STM) [152-153] or CAFM [154]. In this case, the electrical stress can be applied to the STM/CAFM tip, which is placed directly on the RS medium (no top electrode deposition is necessary) to play the role of nanoscale top electrode (see **Figure 9a**). Using STM, lateral atomic resolution has been achieved when measuring ultra thin materials, like graphene [155] (a conductor) and *h*-BN [156] (an insulator). However, such extraordinary ability has never been proven when studying an RS medium. STM has been used to detect enhanced conductivity at the edges of columnar structures in pristine, sputter-deposited silicon-rich  $\text{SiO}_2$  ( $\text{SiO}_x$  where  $x \approx 1.3$ ) [157]. Ref. [157] demonstrated the possibility of switching in a wide spectrum of transition metal

oxides using STM. Other studies include investigations of more advanced material systems [158-166]. Although STM may provide better lateral resolution than CAFM due to the smaller tip radius and its operation in ultra-high vacuum, STM presents three important problems limiting its use in RS studies: *i*) the samples need to show some intrinsic conductivity prior to switching, otherwise it is impossible to measure tunneling current. This dramatically limits STM studies of resistance switching to conductive, leaky or very thin materials; *ii*) the tip-sample distance is measured by evaluating tunneling current across the sample. This is a problem when measuring lateral scans, as one cannot know if a current increase or decrease is related to a change in the conductivity of the material (presence or absence of defects) or to a local topographic fluctuation of the RS medium; and *iii*) it is widely accepted that trustable STM measurements need to be done in ultra high vacuum, which enormously increases the complexity and slows down the overall experiments.

CAFM is a more practical tool that can easily distinguish between topography and conductivity changes, as they are measured independently (the first one using an optical or piezoresistive system to detect the deflection of the cantilever containing the probe tip, and the second one using a current-to-voltage preamplifier [154]). In CAFM experiments the effective area at the tip/sample junction ( $A_{\text{eff}}$ )—this is not the contact area, but the area across which the electrons can flow, which can be different [154]—may range between  $1 \text{ nm}^2$  and  $700 \text{ nm}^2$ , depending on the radius of the tip, stiffness of tip and sample materials, tip/sample contact force, and relative humidity of the environment [44], being  $\sim 50 \text{ nm}^2$  [167] the most common/accepted value. Therefore, the CAFM can be used to prove the presence of RS in ultra-scaled MIM cells. When performing sequences of I-V sweeps to explore RS with a standard CAFM, some essential factors need to be considered: *i*) most commercial AFMs do not allow

applying voltages above  $\pm 10\text{V}$ , which hinders the observation of the forming process in several samples; *ii*) most standard CAFMs just measure currents within 2-4 orders of magnitude. This makes visualizing the set and reset processes impossible, and only the shifts of the I-V sweeps (and their curvature change) can be detected (see Figure 9b). To solve these problems some manufacturers offer the possibility of using a logarithmic preamplifier [168-171] for current evaluation, but that module is expensive and not compatible with all CAFMs; *iii*) no CAFM can apply variable current limitation, which may produce undesired damage during the set process. It should be noted that most CAFMs show current saturation (see horizontal line in Figure 9b), but that not necessarily limits the current flowing across the tip/sample junction [172]; *iv*) measuring bipolar RS in metal oxides using a standard CAFM working in air conditions is very challenging because the relative humidity of the environment produces a water meniscus at the tip/sample junction, which leads to local anodic oxidation (LAO) of the metal oxide [173-174]. Problems *i*), *ii*) and *iii*) can be solved by connecting an SPA directly to the CAFM tip and sample holder, while problem *iv*) can be solved by measuring in dry  $\text{N}_2$  or vacuum atmospheres, which minimize the formation of a water meniscus at the tip/sample junction. The suggested CAFM setup for studying RS via sequences of I-V sweeps is displayed in Figure 9c [46]. Using this setup, both forming and cycling can be *in situ* monitored (see Figure 9d).

It is important to highlight that the CAFM cannot perform reliable endurance tests locally. The reason is that the tip of the CAFM experiences lateral thermal drift [175], which slowly moves it to a different location; we characterized the thermal drift to be  $\sim 10$  nm/hour, although it may differ a lot from one CAFM to another. Moreover, in many cases RS involves large currents up to  $\sim 1$  mA, which implies a current density at the tip/sample junction of  $\sim 10^9$  A/cm<sup>2</sup>, as  $A_{\text{eff}}$  is  $\sim 100$  nm<sup>2</sup> [176]. These ultra high

current densities are very harmful for all CAFM tips, and there is no tip capable of resisting such aggressive stress, even when using solid conductive tips [45] (which may lose their sharp shape due to material melting, and even adhesion of particles at the apex due to thermo-chemical reactions, which kills their conductivity). For these reasons, the maximum number of RS cycles collected at a single location with a CAFM reported is 100 [177-178]; therefore, the CAFM is an excellent tool for elucidating which locations of the sample show RS, but not enough reliable for conducting endurance tests. In Refs. [47-48] a CAFM working in dry N<sub>2</sub> and connected to an SPA was used to demonstrate that the RS in polycrystalline HfO<sub>2</sub> stacks only takes place at the grain boundaries, which are rich in defects [179]. Another important consideration is that the RS parameters measured with the CAFM tip (*i.e.* V<sub>SET</sub>, V<sub>RESET</sub>, I<sub>HRS</sub>) may vary a lot depending on the measurement conditions (*i.e.* environment [44, 180-181], tip diameter [167], contact force [182]). Therefore, fitting one single I-V sweep collected with a CAFM to any tunneling equation is meaningless; such fittings should always be performed statistically [42, 183].

Similar to the sequences of I-V sweeps, the RS can also be studied from sequences of current maps [184-186]. The advantage compared to sequences of I-V sweeps is that the current maps can test much larger areas (typically 1 μm × 1 μm to 10 μm × 10 μm), which allows performing statistical analyses of the size and currents driven by the CFs [185]. Moreover, as the area in which the RS takes place is larger, this can be combined with chemical tools, such as energy dispersive X-ray spectroscopy (EDS) or X-ray photoelectron spectroscopy (XPS), to study the chemical changes involved in the switching [184].

Another interesting possibility is the application of set/reset stresses at the device level and later analyze the local conductivity changes via CAFM maps. Measuring

current maps by placing CAFM tip on the metallic electrode is not a good choice because that may blur the shape and currents driven by the CFs due to the large lateral conductivity of the metal; in other words, the currents driven by one spot can be detected even when the tip is placed on the metal far from it [187], leading to a false CF size. Therefore, the top electrode needs to be removed before the CAFM scan. The main two options reported are: *i*) removing the top electrode via standard dry [188] or wet [186, 189] etching. In fact this was the first type of RS experiment conducted using CAFM [189], and allowed for the first time detecting the changes on the size and resistivity of single CFs. This is the most common method, and it has been also used to remove the gate electrode in field effect transistors to analyze the reliability of the gate oxide after electrical stresses [190]. When using this method it is very important to have a very large etching selectivity between the metallic electrode and the RS medium, otherwise the second one might be damaged, and the subsequent information collected via CAFM may not be accurate; and *ii*) the tip of the CAFM has been used to etch (scratch) the entire top metallic electrode [191], and even the RS medium. While there is no question regarding the etching ability of the CAFM tip [192], the reliability of the associated current measurement is questionable due to fast tip degradation [45, 193], generation of local heats during the physical etching that may change the properties (e.g. phase) of the underlying RS medium, and difficulty of keeping a constant electrical field during the etching (that would require accurately changing the voltage after each scan). More works discussing the effect of these concerns and the overall validity of this technique are required. An interesting novel method is the use of an ionic liquid electrolyte for the device level experiment [194], as it allows being easily rinsed and the surface of the RS medium becomes exposed, perfect for carrying out CAFM

experiments. More detailed explanations about the use of CAFM for the study of RS can be found in Refs. [195-196].

### **3.6. Switching mechanism**

When attempting to discover the physics underlying RS mechanisms through imaging, the overarching principle guiding experimental design must be realism. Real, deployable RS devices are made with certain materials, assembled into a certain geometry with a particular fabrication process, and are switched using some particular electrical stimulus provided by a background support architecture. At present, no imaging technology exists that is capable of peering into a real, unmodified RS device with sufficient spatial resolution to resolve the physical processes of interest. To explore these physical processes, one must arrange improved imaging access, either by modifying a real device, or by building a custom analog. Inevitably the device that can be studied using the preferred imaging technique differs from a real device, if not at the beginning of the experiment, then by its conclusion. These differences can play an important role in dictating the imaged device's function, and in extreme cases can obscure the physics that is the stated target of the entire investigation.

So, the subject of an imaging experiment is necessarily a compromise between the ideal case of a real device, and the feasible case, which employs a device adapted for imaging. Given the necessity of this compromise, one must consider its consequences most carefully during two separate phases of the experimental investigation. First, during the experimental design phase, effort must be made to, within the experimental constraints, make choices that will minimize the potential of these compromises to create differences between the physics that will be observed in the imaged system, and

the physics which occurs in the real, un-imaged system. This step involves both guesswork as to what variables are most critical for maintaining a faithful representation, and also a cost-to-benefit analysis as to how much time, effort, and expense can be dedicated to controlling a given variable. A partial list of issues to consider, sorted into broad categories that necessarily have substantial overlap, is given below.

*Materials:* Materials foreign to a real RS device can be introduced by focused ion beam, electron beam, and ion mill sample preparation, which can deposit or implant such substances as gallium, platinum, electrons, hydrocarbons, or noble gases. Additionally, active interfaces exposed to air can absorb any number of contaminants. Gallium in particular is likely to be a bad actor in a RS study, as it is both conductive and mobile at room temperature and above.

*Geometry:* Geometric discrepancies from a real RS device can be topological or quantitative. In the former category, a topological difference is generated by introducing a new interface or surface that connects the two electrodes. Such an interface allows for surface migration, a transport mechanism that is physically distinct from, and generally faster than, the bulk migration that must occur in many categories of real RS devices. Worse, these interfaces are often both variable and not well characterized: they might represent a layer damaged relative to the bulk during the sample preparation process, or they have been exposed to ambient atmosphere with varying levels of humidity and other contaminants. In the quantitative category, some experiments will scale a critical dimension such as the electrode area or separation for convenience of fabrication or imaging. Often the RS device is scaled toward larger sizes, sometimes by orders of magnitude. In the case of an electron-transparent sample for *in situ* TEM studies, however, the device's thinness can produce an unrealistically small thermal conductance to ambient temperature. Naturally dimensional changes of any sort can

drastically alter, for instance, the statistics of device switching, the switching times, and the switching voltages required.

*Fabrication:* As mentioned above, taking a real RS device and adding additional fabrication steps to prepare it for imaging can compromise the device function. However, while fabricating a custom device purely for the purpose of imaging an RS process (see **Figure 10**) can avoid the need for *extra* sample preparation steps, this approach can, depending on the fabrication process, still introduce possibly problematic discrepancies from real device function. For instance, by physically moving a mechanical probe, which serves as one electrode and might be coated with the barrier oxide, into contact with a counter electrode, one can form a device that shows RS characteristics and is amenable to imaging (Figure 10c). Another possibility is to fabricate an ultra-thin electron-transparent MIM structure and place a mechanical probe on the top electrode (Figure 10b). However, when doing these experiments two important considerations need to be taken into account: *i*) in the first case (Figure 10c), the contact area, which defines the device size, shows a non-negligible degree of uncertainty; and *ii*) in both cases (Figures 10b and 10c) the tip/sample pressure is difficult to control. For this reason, when doing these experiments, it is recommendable first to characterize such parameters doing additional experiments using reference samples [11, 19]. Computational studies may also help to shed light into this issue. Another possibility is to fabricate a horizontal geometry, where both electrodes are deposited in a single step, either underneath or on top of the electrolyte (Figure 10d). As discussed above, this shortcut relative to the real, vertically-stacked RS device fabrication process (where the BE, electrolyte, and TE are put down sequentially) introduces a connecting interface. Of course, custom devices can also be fabricated in such a way that the materials are nominally identical with those found in a real device,

but in practice behave much differently. For instance, a thermally grown oxide electrolyte might or might not perform like one put down with atomic layer deposition.

*Electrical:* In a deployed device RS is affected by nanosecond-scale pulses with volt magnitudes, and the devices can switch millions of times without failure. Typical *in situ* imaging experiments operate in a quasi-DC regime with larger voltages, and manage anywhere from (most commonly) half of one switching cycle to a bare handful of full cycles. Even *ex situ* imaging experiments, which generally have much more realistic architectures, sometimes deliberately apply destructively large switching voltages to create conducting pathways that can be easily located for imaging. Stray capacitance quickly becomes problematic in systems where the switching voltages are generated remotely from the RS device. Minimizing cable lengths can help prevent device destruction. To date the characterization community has failed to image any RS device operating at a realistic speed for a large number of cycles. Clearly there is room for much improved realism in this area.

*Supporting architecture:* Real RS devices are found in arrays, with bit and word lines, and have transistors or some other selector device to mitigate the sneak path problem. Generally *in situ* imaging experiments have made no attempt to incorporate this background architecture. Destructive *ex situ* imaging experiments, on the other hand, have extracted data from entirely realistic cross-point arrays.

*Imaging technique:* In the case of an imaging technique such as scalpel AFM, the act of imaging has a profound and obvious effect –total destruction– on the RS device. The information that can be extracted from such a single snapshot is necessarily limited, a disadvantage counterbalanced by the advantage of the ability to probe an entirely realistic device architecture. However, a recent study reported serious concerns about the reliability of this technique when studying thin dielectrics (which is the case

of RS devices) [193]. With electron microscopy-based imaging, the effects of imaging can be more subtle. Here the importance of cycling devices under both beam-on and beam-off conditions cannot be overstated. The sensitivity of an RS device to the electron beam may depend strongly on the device chemistry, e.g. conductive bridge RAM (CBRAM) or valence change memories (VCM). Cycling also allows one to distinguish between ageing or beam-induced imaging artifacts (e.g. beam-deposited contamination), and the bias-induced effects of interest.

*Thermal considerations:* The operation of RS devices is often controlled by localized self-heating effects, especially in filamentary devices. Understanding heat and energy dissipation is crucial for the evaluation and design of devices (see also Section 4: simulation of RS) since most proposed switching mechanisms rely on thermally-activated processes such as defect generation, ionic transport etc [1]. Several unique structures have been used to evaluate the local temperature in resistive memory devices [197-199], and ultrafast transient electrical measurements were proposed to study an effective device temperature [200]. Yet, detailed understanding of the switching and retention mechanisms in RS devices requires more thermal measurements, particularly spatially resolved temperature measurements in realistic device structures should be pursued. Experimental measurement of the local temperature in nanoscale devices is extremely challenging. The ultrafast transient technique [200] allows measuring realistic device structures but requires sub-nanosecond electrical measurement (or shorter than the thermal transient) and only an effective device temperature is obtained, which may be significantly different from the peak temperature [199]. Scanning thermal microscopy (SThM) [201-202] is a good candidate for measuring spatially-resolved temperature with nanoscale resolution in future work. The main challenges for SThM measurements are the calibration of its signal to device temperature, and the heat

spreading across the top electrode which could limit its spatial resolution. It should be noted that any thermal measurement must also be accompanied by a good electro-thermal model.

*Remarks on experimental descriptions:* The second time to carefully consider the compromises made in an experimental investigation is during the presentation of the results. The authors of an experimental study know well and have thought deeply about the limitations of their methods. It is incumbent upon them, as the experts, to explain in plain terms both their efforts to mitigate the confounding compromises inherent to their experimental design, and where these efforts may have fallen short.

#### **4. Simulation of RS: from material to devices and systems**

In the field of RS, simulations can be used to interpret experimental data, optimize processes and devices, project accelerated test results under specific operation conditions, predict performances, and screen new materials and device architectures. These computations require the use of models linking material properties to devices and circuits performances. Thus, a hierarchical multiscale modeling structure is needed, which is comprised of three main levels that have to be tightly connected; *i*) material properties calculation: atomistic approaches including *ab-initio* methods are used to calculate fundamental material properties and defect characteristics; *ii*) device models: kinetic Monte Carlo (kMC) and finite elements methods (FEM) models are used to project the material properties into the electrical performances of devices, including variability and reliability; *iii*) semi-empirical/compact models: they are used in circuit simulations to assess the circuit/system performances starting from individual device characteristics. In this section, the main advantages and limitations of the different

simulation approaches are discussed, including the experimental input needed for their calibration and verification.

#### **4.1. Microscopic models**

Atomistic models are paramount for better understanding of the physical processes in RS devices, such as creation, recombination, and diffusion of defect species, and their role in the switching and charge transport mechanisms (e.g., CF formation and dissolution, evolution of material's structure, heat dissipation, and electrical conduction through these structures) [203-204]. Such models should account for the charge transport and the phenomena leading to RS. To properly catch the physics of RRAM devices regardless of their composition and resistive state, microscopic models should include three main components: *i*) the relevant defects-, atoms-, and materials-related phenomena (generation, recombination, drift, and diffusion of defects/atoms, clustering effects, structural and phase changes in the materials and related electrical/thermal/optical properties, reactions at interfaces) as well as their interplay [205]. *ii*) Electron and ion transport models, including carrier tunneling mechanisms, defects sub-band creation, and generalized Landauer approach/ballistic transport. *iii*) Finally, a (kinetic) Monte Carlo engine should be included to account for the inherent stochasticity of defects-related phenomena and simulate their evolution.

Available experimental information on the physical and chemical properties of materials (e.g., crystallographic and band structure, thermal conductivity, band-gap, work function) can be used for calibration of these models. The properties of the most relevant defects in each material (e.g. activation energies for the creation and recombination of defect species, their mobility within the insulator, defects thermal

ionization and relaxation energies) are typically calculated using Density Functional Theory (DFT) and molecular dynamics (MD) simulations and can be compared to the results of electrical characterization experiments (e.g., time-dependent dielectric breakdown, variable ramp-rate and temperature switching, random telegraph noise characterization).

This approach can provide a more detailed understanding of the complex physics underlying formation of CFs in different materials [205-208] and thus help to design devices for specific applications [209]. It can help to identify which material is best-suited for a given target application and provide a useful reference to calibrate appropriate semi-empirical and compact models. To use this approach, one does not require preliminary knowledge of the structure of CF, and it can handle complex material structures exhibiting multilayers (which are extensively investigated and proposed in the literature). On the other hand, creating these comprehensive and complex models requires significant simulation time (several days to several months) and the use of large sets of possible combinations of configurations and structural effects (in some cases not so well defined). Due to these limitations, it is critical to understand which particular processes to include into the model and which could be safely excluded in order to obtain meaningful results while minimizing the simulation time. In many cases, such simulations are impossible without using high-capacity computational systems, which makes these models difficult to employ for simulations of circuits and systems.

#### **4.2.2. kMC/FEM models**

The simulation of the electrical characteristics of RS devices requires numerical models based on the 3-D FEM and kMC approaches. Besides simulating the electrical device behavior, both models allow reproducing the physical phenomena occurring in RS devices during operation and reliability tests.

FEM models simulate electron, ion, and heat transport by differential equations based on quasi-classical models, Poisson's equation for the electric field distribution and current continuity, Fourier's law for heat generation/diffusion, and a drift-diffusion model to describe ionic motion [210]. Density gradient induced diffusions and electric field driven drifts control the ionic migrations occurring by hopping across energy barriers determined by DFT methods. This thermally-activated ion-migration process emphasizes the key role played by the temperature, which accelerates the ionic migration, thus requiring a careful simulation of Joule heating effects [211-214]. This is particularly relevant for filamentary switching, where electrical conduction is strongly confined at a conductive filament, CF. Defects such as oxygen vacancies and metallic impurities act as dopants for the oxide film, hence their migration can result in a change of CF shape, which in turn affects the device conductivity [215-217].

kMC models represent another approach to simulate the electrical characteristics and physical processes happening in RRAM devices. The main difference compared to FEM models is that kMC models account for the individual contributions of defects/ions/vacancies, which allows simulating variability and reliability including statistics. Among the physical processes considered beyond those already accounted for by FEM models, it is worth mentioning the generation and recombination of oxygen vacancies, which play a crucial role in both forming and switching, and trap assisted tunneling (TAT), which is the main charge transport mechanism before forming and in reset conditions [218-219].

Both FEM and kMC models have been shown to accurately agree with a broad range of experimental characteristics, including set and reset transitions under DC and pulsed conditions [220-221]. Typically, FEM allows describing the average device behavior, whereas kMC methods can capture current fluctuations and RS variability. In addition, kMC models can also describe the forming operation, allowing avoiding any assumption on the CF shape/composition considered in switching simulations [222]. Both FEM and kMC models require input material parameters calculated using DFT calculations, and need to be calibrated on electrical device characteristics.

### **4.3. Semi-empirical/compact models**

The development of RRAM based circuits and systems requires compact RRAM device model running in Spice-like simulation environment [223-228]. These compact models rely on conceptual simplifications (e.g. the idea of a conductive filament with a given shape, e.g. cylindrical or conical) and physical assumptions inferred from empirical measurements [101, 229-230]. A variety of semi-empirical models have been proposed, which assume that the CF/s in RRAMs behaves as: *i*) an ohmic conductor, *ii*) an hourglass-shaped quantum-point contact, *iii*) a space-charge region, *iv*) a semi-conductive region that may create a Schottky junction with the electrodes, *v*) a highly-defective region in the dielectric in which either hopping conduction or de-localized transport may occur. The charge transport mechanism can be estimated by fitting the shape and magnitude of the I-V sweeps obtained in the experiments (in both LRS and HRS) using models formulated using compact expressions, such as Schottky or Poole-Frenkel emission, variable- or fixed-range hopping, Landauer formula (ballistic transport), Ohm's law, and tunneling (direct, Fowler-Nordheim or trap-assisted). The

switching mechanisms, properly modeled using FEM and/or kMC approaches, can be included by simplifying the differential equation modeling ion/vacancy motion, generation, and recombination using empirical expression accounting also for the voltage and temperature dependence of the physical processes [227-228, 232-233].

Compact models are calibrated on FEM/kMC simulations and I-V sweeps measured under different conditions, which depends also on model parameters (e.g., Schottky barrier height, Poole-Frenkel barrier, hopping range, number of open Landauer channels, CF resistivity thermal resistance and capacitance, among others).

## **5. Discussion, perspectives and challenges**

Although RS is a phenomenon known for over half a century [10], research in RS devices did not become exhaustive and widespread until 2008. During the last decade RS devices have been improved in terms of size, switching speed, power and energy consumption, endurance, and data retention. Some RS based devices have been commercialized (but still limited to small-capacity embedded memory of microcontrollers). While developing RS based NVMs for massive information storage still remains a challenge, mainly due to spatial and temporal variability problems, solving those challenges will bring enormous benefits to computing systems (e.g. reduce fabrication costs and enhance information storage performance). Furthermore, RS devices are expected to revolutionize the field of neuromorphic computing, as they can be used as electronic synapses in artificial neural networks. For these reasons, it is expected that RS devices will be a topic of intense research during the next decade.

During the past ten years a large number of RS studies have been reported. Unfortunately, we observed that many of them: *i*) don't provide enough information to

reproduce the experiments, *ii*) use device structures that are not relevant/realistic from a technological point of view, *iii*) omit essential figures of merit, or *iv*) make claims that are not well supported by rigorous experimental or computational data. As a guide for RS scientists, **Table 2** summarizes the essential information that an ideal RS study should include.

When fabricating a RS test structure, small device areas are preferred. Using a substrate that serves as common electrode and large ( $>25 \mu\text{m}^2$ ) top electrodes is not a good practice because the information obtained on a very large device may not be applicable to smaller devices of sizes relevant to real applications, especially in HRS ( $I_{\text{HRS}}$  and  $V_{\text{SET}}$ ). If that cannot be avoided one needs to prove the presence of RS at the nanoscale using experimental techniques (CAFM or *in situ* TEM). The use of planar devices (which work under electromigration or grain boundaries modification phenomena) is not realistic for technological applications due to their large size, high cell-to-cell variability and difficulty to control the switching. We note that in several RS papers (unfortunately too many) essential information about the fabrication of the devices is missing, for example: *i*) the lateral size of the vertical MIM cells, and *ii*) the composition of the electrodes/dielectric. The first case is typical of some authors based at universities, who use large MIM sizes (due to the lack of photolithography or EBL in their labs) and neglect to discuss the device size as an important weakness. Some works vaguely mention the MIM cell size in the supporting material, while it should be clearly stated in the main text. Actually, the MIM cell size is so important that some authors even indicate it in the title [58], which is appreciated. And the second is more typical in reports coming from some companies, which intend to advertise their work without disclosing proprietary information. More open disclosure of key process information will only help to advance this field.

When characterizing a device, it is important to provide enough data supporting the usefulness of the RS mechanism, and these data need to be collected in a rigorous manner. The main problem that we observed in this direction is the lack of figures of merit in several papers. We would like to emphasize again that displaying one/few I-V sweeps showing set and reset transitions does not demonstrate the presence of RS in a MIM cell, even if the authors use a new material and aim at showing a proof-of-concept. RS devices are much more sophisticated than that, and competent RS studies must include endurance, retention, speed, power, energy, scalability, and variability information. Moreover the switching mechanism must be discussed using experimental and/or computational evidences, instead of speculative schematics without any scientific data that supports them. Schematics and drawings claiming the movement of atoms inside the MIM cell must be supported by atomic scale chemical analyses or computational studies, otherwise they are simple speculations and should be understood as such. The most important figure of merit missing in most RS papers is the variability, which is especially important in works claiming multilevel RS observations. Finally, in some cases, we observed that the characterization methods used to assess the figures of merit are not the most appropriate. In this direction, the use of current-blind PVS in incipient MIM structures is one of the most remarkable problems. While this method is valid for well established devices, in prototype devices made of novel materials it should be avoided; in these cases current-visible PVS are highly recommended.

## **6. Conclusions**

The study of RS phenomena and RS devices can be accomplished in several different ways, and therefore the usefulness and impact of the findings reported will be

different. Impactful RS studies should be performed in small ( $<25 \mu\text{m}^2$ ) cells, preferably with cross-bar structure but also including information about isolated cross-point devices. It is strongly recommended to study the RS locally using CAFM and TEM, and such analyses become mandatory when the area of the devices analyzed is  $>25 \mu\text{m}^2$ . The material interfaces need to be flat (RMS  $<400$  pm), clean and, to the extent possible, free of oxygen and moisture from the environment.

The main figures of merit to present in a RS study are: *i*) endurance plot, typically  $R_{\text{HRS}}/R_{\text{LRS}}$  vs. cycle. It is important to conduct experiments that measure the  $R_{\text{HRS}}/R_{\text{LRS}}$  in each cycle, and claiming endurance of millions of cycles but showing endurance plots with few and very spaced data points should be avoided when working with prototypes (current-blind PVS combined with DC measurement of the state resistance should be used only in optimized devices at the industrial stage). Current-visible PVS is highly recommended. *ii*) State retention plot, typically an I-t curve. It is important to indicate the read voltage and the temperature used during the CVS applied for collecting the I-t curve, as well as current limitation used during the state transition (I-V sweep or PVS experiment applied right before to the I-t curve). *iii*) Switching time and energy consumption, which can be calculated in the same experiment. This experiment requires the use of PVS, and if any series device (resistor, transistor) is connected, its location (internal/external) should be described. *iv*) Variability. Information about how many devices were measured, number of cycles per device and dispersion of the main RS parameters ( $V_{\text{SET}}$ ,  $V_{\text{RESET}}$ ,  $I_{\text{HRS}}$ ,  $I_{\text{LRS}}$ ) is necessary, and mandatory in multilevel devices. This is of utmost importance, as variability is the main problem of RS technologies. *v*) Switching mechanism. Although it is very complex, the atomic rearrangements producing the transition between HRS and LRS and vice versa should be analyzed. In situ TEM combined with chemical analyses is recommendable.

Drawing schematics without any nanoscale experimental evidence is just a mere speculation, and should not be interpreted as such. Furthermore, the use of multilevel computational methods is strongly recommended to complement the experiments and gain additional knowledge about the switching mechanism.

Except in the case of variability information (which should always be provided), failing to provide one of these figures of merit in a RS study might be acceptable, as collecting such large amount of data sets may not be possible for all researchers. What should be avoided by all means is to make exaggerated claims based on insufficient experiments, as that produces false knowledge (e.g. overestimation of endurance and state retention time). But the starting point is always a correct device fabrication, otherwise all the experiments coming later might be irrelevant. Adopting these recommendations in future RS reports would help the scientific community evaluate their real usefulness and impact, serving the overall development of reliable RS technology

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## List of acronyms

1T1R	1-Transistor/1-Resistor
2D	Two-dimensional
3D	Three-dimensional
$A_{\text{eff}}$	Effective Area
ALD	Atomic Layer Deposition
BE	Bottom Electrode
BD	Breakdown
CAFM	Conductive Atomic Force Microscope
CBRAM	Conductive-bridging Random Access Memory
CF	Conductive Filament
CL	Current Limitation
CMOS	Complementary Metal-Oxide-Semiconductor
CVD	Chemical Vapor Deposition
CVS	Constant Voltage Stress
DFT	Density Functional Theory
EBE	Electron Beam Evaporation
EBL	Electron Beam Lithography
EDS	Energy Dispersive X-ray Spectroscopy
FEM	Finite Element Method
<i>h</i> -BN	Hexagonal Boron Nitride
HRS	High Resistive State
kMC	Kinetic Monte Carlo
LAO	Local Anodic Oxidation

LRS	Low Resistive State
MD	Molecular Dynamics
MIM	Metal/insulator/metal
MIS	Metal/insulator/semiconductor
MoS <sub>2</sub>	Molybdenum Disulfide
MoSe <sub>2</sub>	Molybdenum Diselenide
NMTRI	Non-volatile Memory Technology Research Initiative
NVM	Non-volatile Memory
PCM	Phase Change Memory
PSV	Pulsed Voltage Stress
PtSe <sub>2</sub>	Platinum Diselenide
RMS	Root Mean Square
RRAM	Resistive Random Access Memory
RS	Resistive Switching
RVS	Ramped Voltage Stress
SEM	Scanning Electron Microscopy
SPA	Semiconductor Parameter Analyzer
SThM	Scanning Thermal Microscopy
STM	Scanning Tunneling Microscopy
TAT	Trap Assisted Tunneling
TDDB	Time-dependent Dielectric Breakdown
TE	Top Electrode
TEM	Transmission Electron Microscopy
TMDs	Transition Metal Dichalcogenides
TMOs	Transition Metal Oxides

VCM	Valence Change Mechanism
WS <sub>2</sub>	Tungsten Disulfide
WSe	Tungsten Selenide
XPS	X-ray Photoelectron Spectroscopy

**Table 1:** Technology requirements for RS based NVMs vs. best performances reported for RS based NVMs. The  $I_{ON}/I_{OFF}$  ratio is not strictly a technology requirement, but it is a reference parameter usually compared in RRAMs. Reproduced with permission from Ref. [7], Copyright Wiley-VCH, 2017. The column "Ref." refers to the references of the paper from which it was extracted (that is Ref. [7]).

Parameter	Technology requirements	TMOs based RRAMs		
		Best performances	Device structure	Ref.
Operating voltages	< 1V	0.3V	Ti/HfO <sub>2</sub> /TiN	41
		0.1V	Pt/Ni/Al <sub>2</sub> O <sub>3</sub> /SiO <sub>2</sub> /Si	43
		-0.2V (set) / 0.5V (reset)	Pt/TiO <sub>2</sub> /Pt	111
Power consumption	~ 10 pJ/transition	0.1 pJ/transition	TiN/Hf/HfO <sub>x</sub> /TiN	31
		0.1-7 pJ/transition	Al/Ti/Al <sub>2</sub> O <sub>3</sub> /s-CNT	44
Switching time	< 10 ns/transition	300 ps	TiN/TiO <sub>x</sub> /HfO <sub>x</sub> /TiN	32
		<10 ns	Al/Ti/Al <sub>2</sub> O <sub>3</sub> /s-CNT	44
		~ ns level	Cu/Al <sub>2</sub> O <sub>3</sub> /aSi/Ta	45
Endurance	>10 <sup>9</sup> cycles	10 <sup>12</sup> cycles	Pt/Ta <sub>2</sub> O <sub>5-x</sub> /TaO <sub>2-x</sub> /Pt	33
		5 × 10 <sup>9</sup> cycles	Pt/TaO <sub>x</sub> /Pt	364
		>10 <sup>12</sup> cycles	Ta/TaO <sub>x</sub> /TiO <sub>2</sub> /Ti	111
		10 <sup>10</sup> cycles	Pt/TaO <sub>x</sub> /Ta	346
		10 <sup>11</sup> cycles	W/AlO/TaO <sub>x</sub> /ZrO <sub>x</sub> /Ru	347
Data retention	>10 years	>10 years @ 85°C	Pt/Al <sub>2</sub> O <sub>3</sub> /HfO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub> /TiN/Si	46
		>10 years @ 85°C	Pt/TaO <sub>x</sub> /Pt	364
MIM cell Size	576 nm <sup>2</sup>	5 nm <sup>2</sup>	TaN/TiN/Zr/HfO <sub>2</sub> /CAFM tip	296
		10 nm × 10 nm	TiN/Hf/HfO <sub>x</sub> /TiN	31
$I_{ON}/I_{OFF}$ ratio	10 <sup>6</sup>	3 × 10 <sup>6</sup>	Ni/GeO/STO/TaN	348
		2 × 10 <sup>6</sup>	Pt/Gd <sub>2</sub> O <sub>3</sub> /Pt	350

**Table 2:** Ideal list of parameters to be provided in a RS study.

Parameter	Recommendation
Device structure	<ul style="list-style-type: none"> <li>• Cross-bar recommended (<i>Figure 1c</i>), cross-point is also OK (<i>Figure 1b</i>)</li> <li>• Common BE structure only if unavoidable</li> <li>• Planar structures are not competitive, should be used only for <i>in situ</i> TEM characterization</li> </ul>
Thin films deposition	<ul style="list-style-type: none"> <li>• Don't pattern electrodes using silver paint</li> <li>• Don't form oxides by exposure to natural air</li> <li>• Indicate the thickness of both electrodes and RS medium</li> <li>• Clarify if the devices were purchased or self made</li> </ul>
Device area and scalability	<ul style="list-style-type: none"> <li>• Clearly state the lateral size of the MIM cells in the main text</li> <li>• Area <math>&lt;10^4</math> nm<sup>2</sup> is recommended (<i>see Figure 1d</i>)</li> <li>• Area <math>&lt;25</math> <math>\mu</math>m<sup>2</sup> is strongly recommended (<i>see Figure 1b</i>)</li> <li>• If device size <math>&gt;25</math> <math>\mu</math>m<sup>2</sup>, CAFM (<i>Figures 9a and 9d</i>) or <i>in situ</i> TEM (<i>Figure 10</i>) are needed to demonstrate scalability of the RS</li> </ul>
Electrical characterization setups	<ul style="list-style-type: none"> <li>• Use integrated resistors or transistors to limit the current (<i>Figure 7a</i>) is better than the current limitation of the SPA (due to overshoot problem)</li> <li>• When using CAFM, logarithmic preamplifier or external SPA connection is recommended to apply/measure high voltages/currents (<i>Figure 9c</i>). For bipolar RS on oxides, the use of N<sub>2</sub> or vacuum chambers is necessary (<i>Figure 9c</i>)</li> <li>• If CAFM is used, indicate the properties of the tip (material, tip radius, spring constant) and atmosphere. Solid metallic probes are recommended</li> </ul>
Endurance	<ul style="list-style-type: none"> <li>• Indicate if R<sub>HRS</sub>/R<sub>LRS</sub> was studied via I-V sweeps, current-visible PVS or current-blind PVS. Always indicate the pulse sequence used</li> <li>• Current-visible PVS (<i>Figure 5b</i>) is highly recommended for the first 10<sup>6</sup>-10<sup>7</sup> cycles. When measuring endurance <math>&gt;10^7</math> cycles, current-blind PVS may be used to keep a low testing time.</li> <li>• When using current-blind PVS to study extreme endurance, acquiring <math>&gt;50</math> R<sub>HRS</sub>/R<sub>LRS</sub> data points per decade is necessary</li> <li>• Claiming endurance of millions of cycles showing endurance plots with few (<math>&lt;100</math>) very spaced data points (<i>Figure 5c</i>) is NOT OK, especially when working with prototype devices using novel materials. In such devices R<sub>HRS</sub> and R<sub>LRS</sub> should be measured in each cycle (<i>Figure 5b</i>)</li> </ul>
State retention	<ul style="list-style-type: none"> <li>• Indicate the current limitation used for the set (<i>Figure 6a</i>)</li> <li>• Indicate if high temperatures were used or not (<i>Figure 6b</i>)</li> <li>• Indicate the read voltage</li> <li>• In electronic synapses, statistical study of the relaxation is necessary (<i>Figure 6c</i>)</li> </ul>
Switching time and energy consumption	<ul style="list-style-type: none"> <li>• Carefully describe the setup used for this measurement (<i>Figure 7a</i>)</li> <li>• Indicate the minimum time detectable with your setup (resolution)</li> <li>• Monitor several cycles of set/reset current (<i>Figures 7b and 7c</i>)</li> </ul>
Variability	<ul style="list-style-type: none"> <li>• Indicate how many devices were measured</li> <li>• Indicate how many cycles per device were measured (<i>Figures 8a and 8b</i>)</li> <li>• Indicate what is the dispersion of V<sub>SET</sub>, V<sub>RESET</sub>, I<sub>HRS</sub>, I<sub>LRS</sub> from cycle-to-cycle and from cell-to-cell (<i>Figure 8</i>)</li> <li>• In multilevel devices cell-to-cell variability information is mandatory</li> </ul>
Switching mechanism	<ul style="list-style-type: none"> <li>• <i>In situ</i> atomic scale chemical studies are recommended (<i>Figure 10</i>)</li> <li>• Indicate the thickness of the lamella used in the TEM</li> <li>• Schematics describing RS without atomic scale chemical measurements is just an speculation, not a demonstration</li> <li>• Indicate the lateral resolution of the technique used</li> </ul>
Simulation	<ul style="list-style-type: none"> <li>• Indicate the models and numerical methods used (<i>Figure 11</i>)</li> <li>• Indicate the assumptions made</li> <li>• Indicate the simulation time</li> </ul>

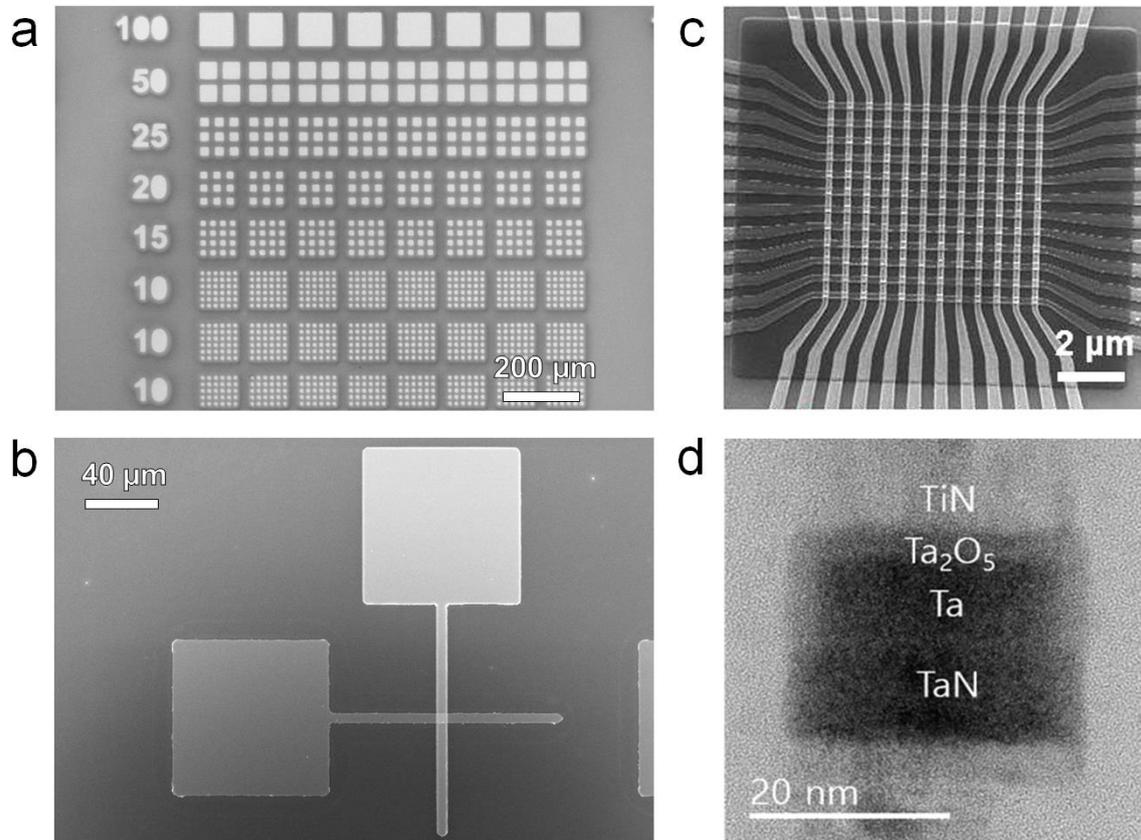


Figure 1: Common structures for the study of RS devices. SEM images of the three main types of structures commonly used to study resistive switching. (a) TE deposited on blanket samples with a common BE, (b) Isolated cross-point RS devices, (c) cross-bar structure formed by multiple cross-point structures interconnected. (d) Cross-sectional TEM image of a 28 nm wide MIM structure. (a) and (b) are reproduced with permission from Ref. [41], copyright Wiley-VCH 2018. (c) is reproduced with permission from Ref. [54], copyright Springer Nature 2016. (d) is reproduced with permission from Ref. [59], copyright Royal Society of Chemistry 2017.

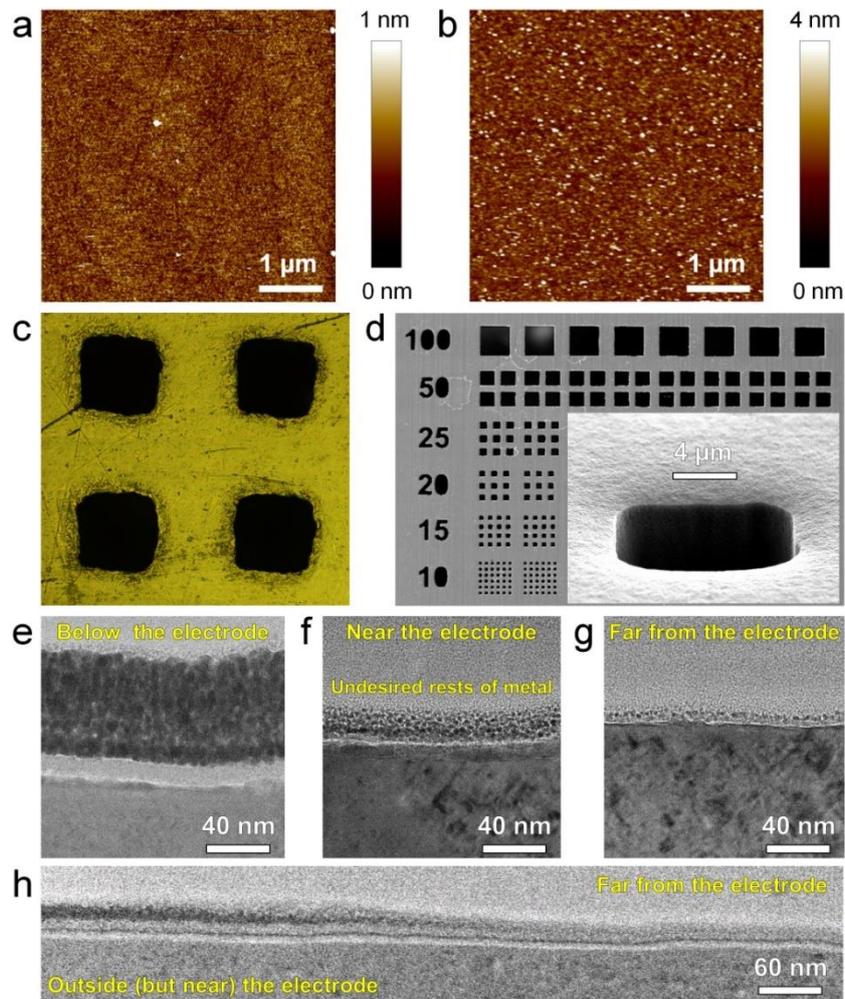


Figure 2: Using photolithography vs. shadow mask. Topographic AFM maps of the surface of a Si wafer (a) as-purchased and (b) after deposition and removal of a photoresist (before metal deposition). Despite intense cleaning, the surface always includes some rests of photoresist residues that are impossible to avoid. (c) Optical microscope photograph of a standard shadow mask patterned mechanically. The size of the holes is  $50\ \mu\text{m} \times 50\ \mu\text{m}$ . (d) SEM image of a laser patterned shadow mask. The inset shows a zoomed image of the hole. (e), (f) and (g) are the cross sectional TEM images collected in a sample like that of Figure 1a, below, near and far from the electrode (respectively). (h) Large-area SEM image of an area outside (but near) the electrode. Panels (e)-(h) demonstrate that using a shadow mask rests of metal can penetrate below it, propagating below the shadow mask ( $<1\ \mu\text{m}$ ).

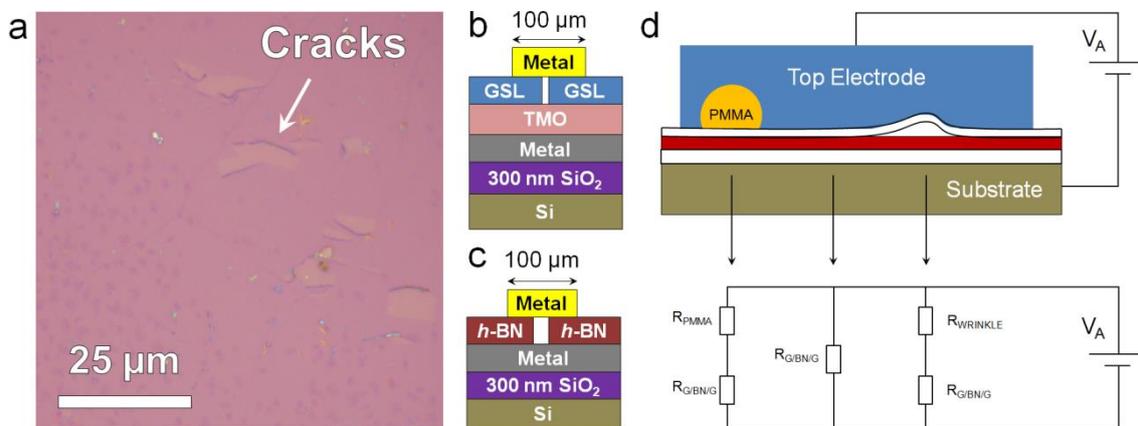


Figure 3: Fabrication issues of RS cells made of 2D materials. (a) Optical microscope image of a single layer graphene sheet with several cracks, wrinkles and multilayer islands. When transferring ~6 layers thick graphene using exactly the same method a much lower amount of cracks (in some cases even negligible) has been observed. Schematic of (b) a metal/*h*-BN/metal and (c) a metal/graphene/TMO/metal RS device. If the 2D material is monolayer the formation of cracks is much easier, and this would produce shorted devices in the metal/*h*-BN/metal ones, and accumulation of CFs at the cracks in the metal/graphene/TMO/metal ones. (d) Schematic (top) and equivalent electrical circuit (down) of a Metal/graphene/insulator/graphene/metal RS cell under bias ( $V_A$ ). The cell includes one polymer (PMMA) residue and one wrinkle. The schematic indicates that the RS event will never take place at those locations, as the BD (CF formation) takes place at the weakest location of the sample, and they are more resistive.

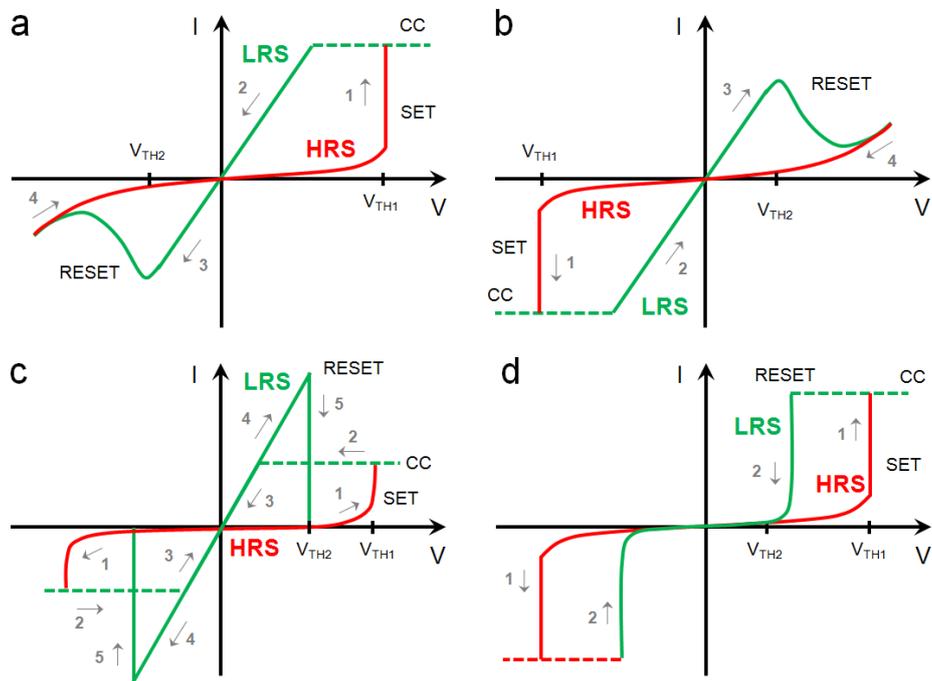


Figure 4: Types of RS characteristics. (a), (b) Typical I-V sweeps showing one cycle of and bipolar RS, inducing the set with positive and negative polarities (respectively). (c), (d) Typical I-V sweeps showing the presence of and unipolar and threshold RS (respectively). For bipolar RS one entire cycle expands to two quadrants of the Cartesian axis (1<sup>st</sup> and 3<sup>rd</sup>), while unipolar and threshold are confined to only one, which can be either the 1<sup>st</sup> (positive set) or the 3<sup>rd</sup> (negative set). (a) and (b) are modified and reprinted with permission from Ref. [1], copyright Wiley-VCH 2016.

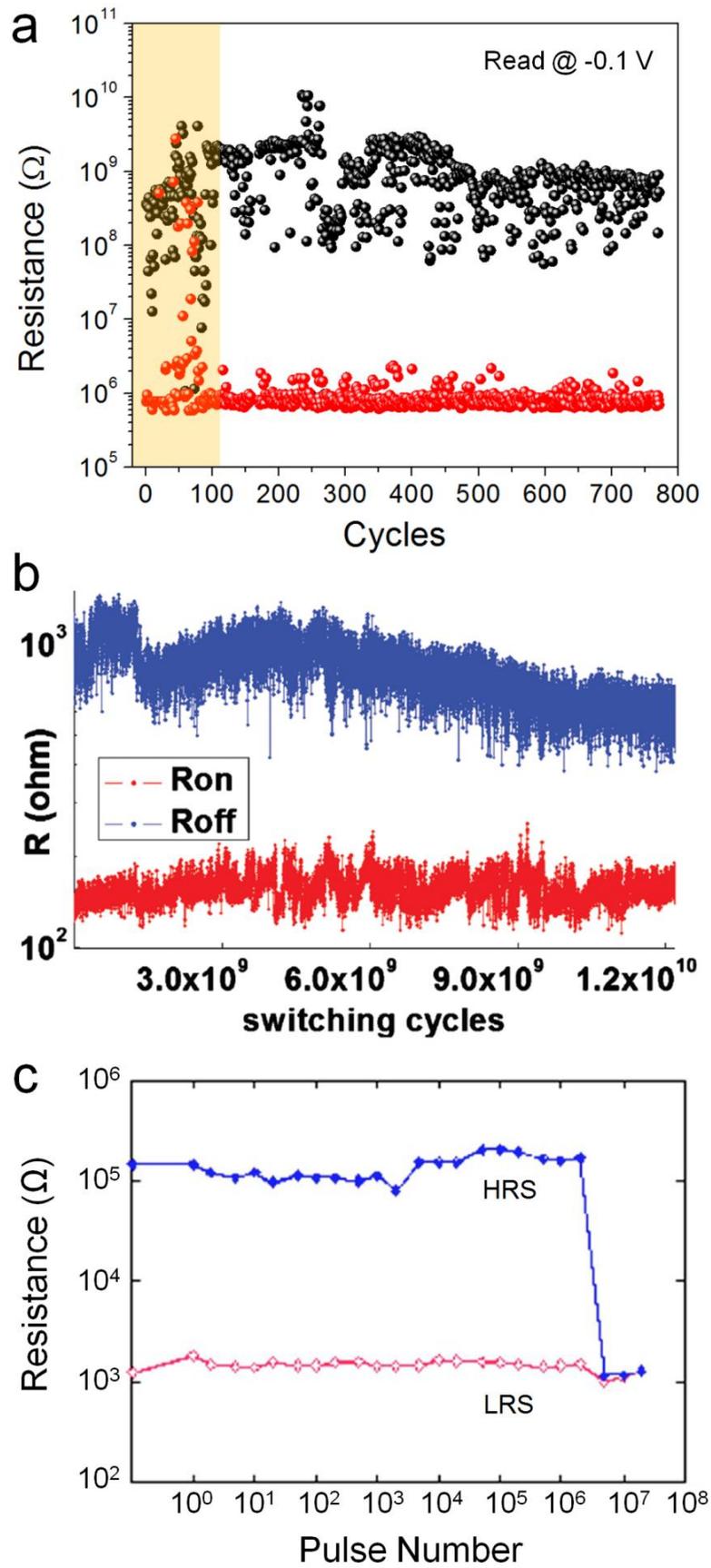


Figure 5 (see caption in next page)

Figure 5: Endurance plots collected by three different methods. (a) By measuring several I-V curves and extracting the resistance at  $-0.1\text{V}$ . (b) By using pulse stresses recording the current simultaneously and calculating the resistance for each cycle (namely current-visible PVS). (c) By using pulsed stresses without measuring the current simultaneously (namely current-blind PVS). The resistance is extracted by stopping the tests and collecting one I-V curve, and extracting the value of the resistance in that specific cycle. Method (a) is too slow and the stresses applied do not correspond to the real functioning of the devices, although it can prove switching in each single cycle. Method (c) is faster uses realistic stresses, but it cannot properly prove the switching in all the cycles. Method (b), which is the recommended one, is faster and proves the switching in each single cycle. (a) is reproduced with permission from Ref. [9], copyright Wiley-VCH 2017. (b) is reproduced with permission from Ref. [114], copyright American Institute of Physics 2010. (c) is reproduced with permission from Ref. [13], copyright American Institute of Physics, 2007.

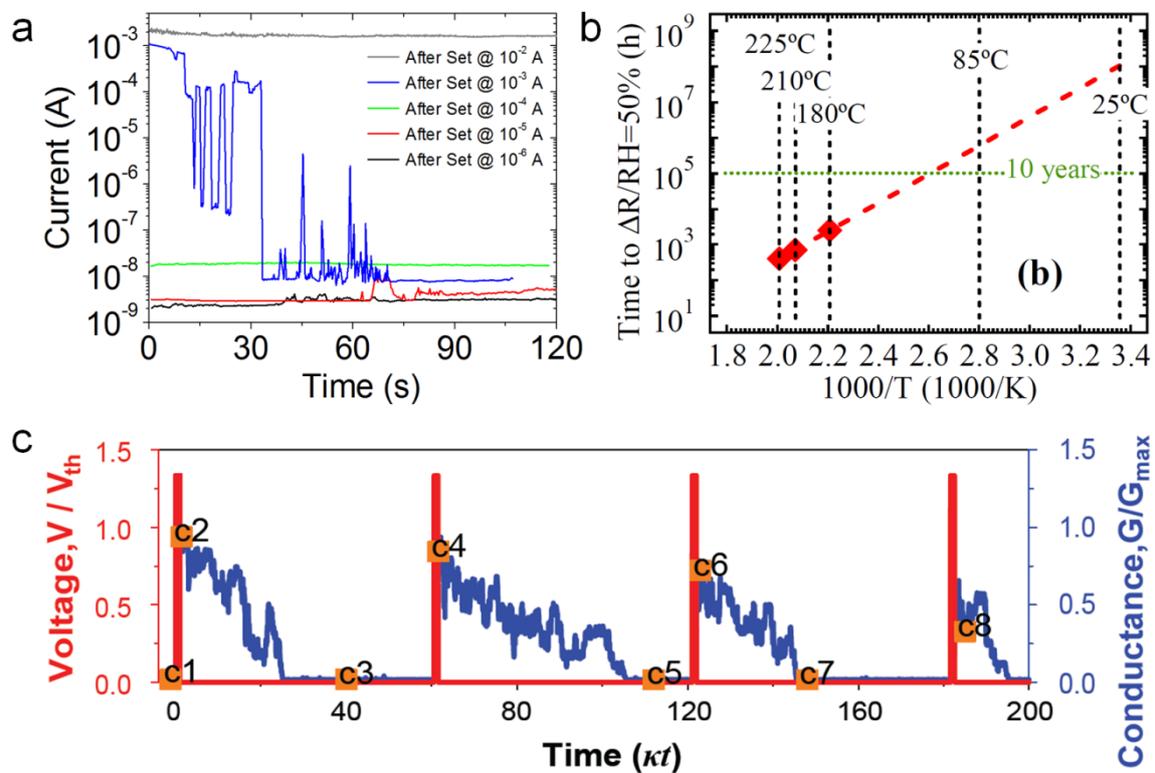


Figure 6: Measuring the retention and relaxation times of RS devices. (a) I-t curves, collected using  $V_{READ} = 0.1$  V, showing the retention of the LRS; as it can be observed, it strongly depends on the current limitation used. (b) Arrhenius plot of data retention properties of TaOx memory cells. (c) Use of pulsed tests to monitor the relaxation of RS devices showing threshold type RS. This test is especially useful to study RS devices for neuromorphic applications and short term plasticity. (a) is reproduced with permission from Ref. [22], copyright IEEE 2018. (b) is reproduced with permission from Ref. [127], copyright IEEE 2008. (c) is reproduced with permission from Ref. [132], copyright Springer Nature.

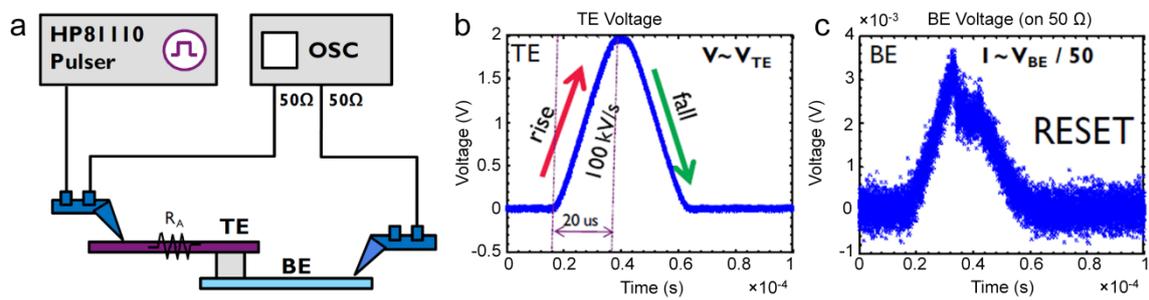


Figure 7: Switching time and Energy consumption. (a) Schematic of the setup recommended for the characterization of the switching time and energy in RS devices. The bias is applied using a pulse generator, and a series resistor is used to limit the current across the device in LRS. (b) Voltage and (c) current signals be measured with the oscilloscope. Reproduced with permission from Ref. [138], copyright IEEE 2012.

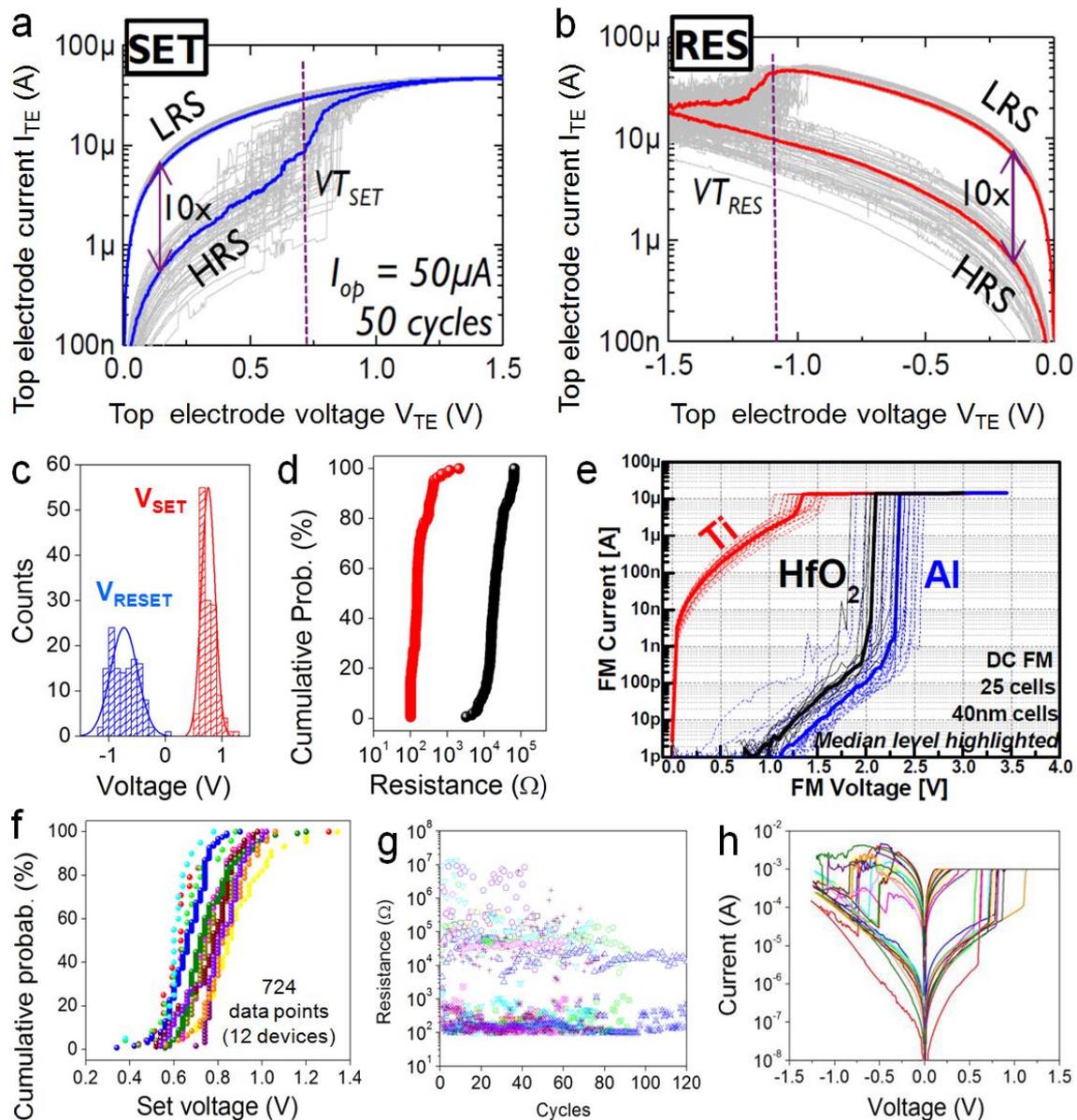


Figure 8: Statistical analyses to evaluate variability of RS devices. (a) and (b) I-V sweeps showing the typical bipolar RS behavior during 100 cycles. (c) shows the histogram of  $V_{SET}$  and  $V_{RESET}$  for 100 I-V sweeps measured in the same device. (d) shows the histogram of  $R_{HRS}$  and  $R_{LRS}$  for 100 I-V sweeps measured in the same device. (e) I-V sweeps collected in different groups of devices; the median of each group (Ti, HfO<sub>2</sub>, Al) is highlighted in bold. (f) Superimposed cumulative probability plot of  $V_{SET}$  for 12 different devices. (g) Endurance plot of 7 devices superimposed (empty symbols correspond to  $R_{HRS}$  and crossed symbols to  $R_{LRS}$ ). In this plot only 100 cycles have been

plot for clarity, as the goal is to analyze the variability. (h) Median I-V sweep of 15 devices; for each device at least 100 cycles were measured. (a) and (b) are reproduced with permission from Ref. [142], copyright IEEE 2014. (e) is reproduced with permission from Ref. [143], copyright IEEE 2014.

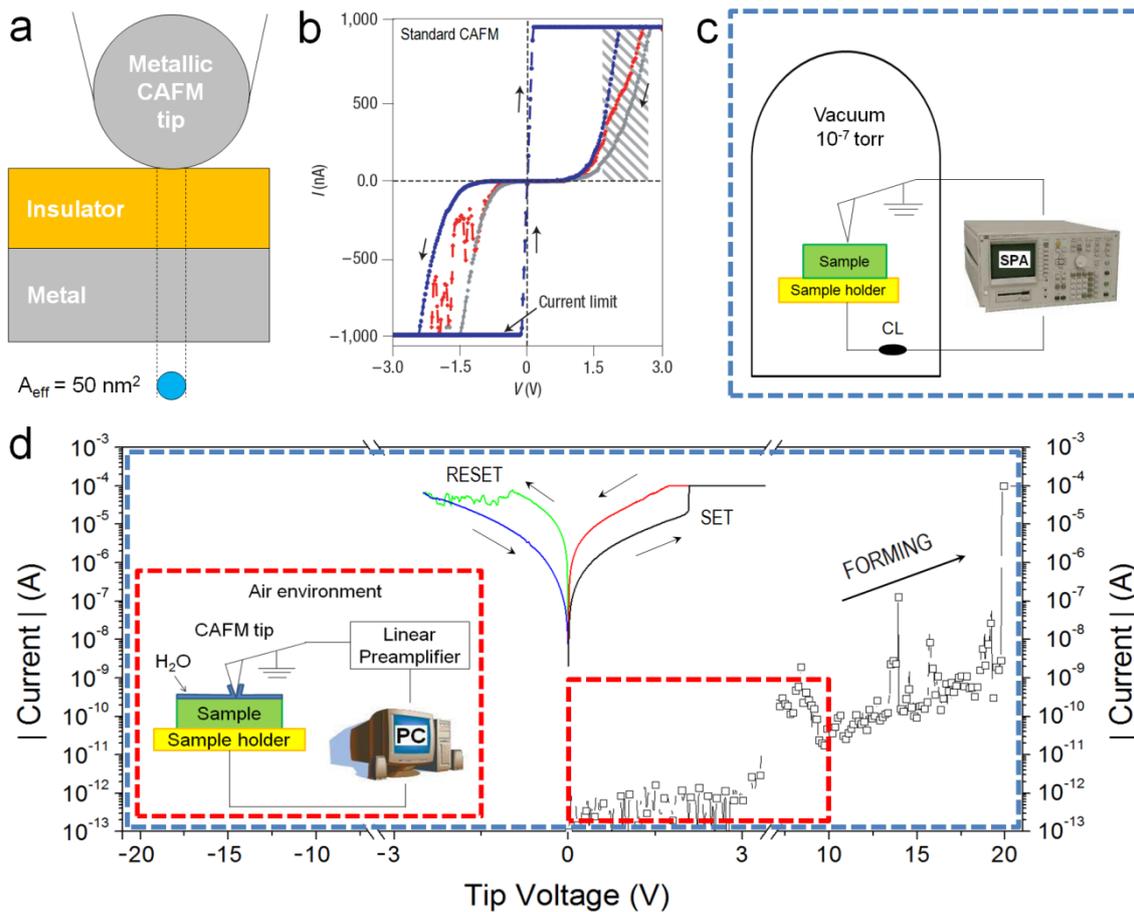


Figure 9: Nanoscale study of RS using CAFM. (a) Schematic of a nanosized MIM structure using the tip of the CAFM as top electrode. (b) Typical IV curves collected with standard CAFMs showing RS. The set and reset processes cannot be observed, just shifts. (c) block diagram of an SPA connected to a CAFM tip working in vacuum for nanoscale bipolar RS characterization. This is the recommended setup for nanoscale RS characterization. (d) I-V curves showing bipolar RS behavior, which have been collected with the setup shown in panel (c). The blue dashed line is the voltage and current range covered by the setup shown in panel (c) can work. The inset shows the block diagram of a standard CAFM, which can only measure the window highlighted with red dashed lines. (b) is reproduced with permission from Ref. [234], copyright Springer Nature. (c) and (d) are modified and reprinted with permission from Ref. [46], copyright The Electrochemical Society.

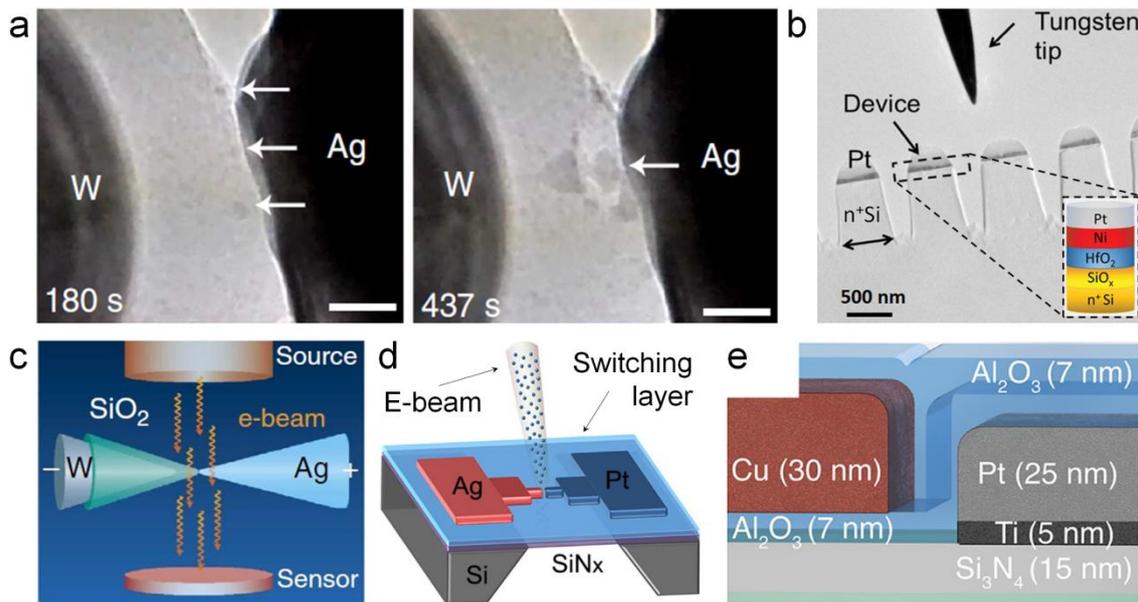


Figure 10: *In situ* TEM characterization of RS. (a) TEM image of a W/SiO<sub>2</sub>/Ag structure after being polarized for 180 s and 437 s at 8V, showing the formation of a CF across the dielectric. The scale bars in (a) are 20 nm. (b) TEM image showing a tungsten tip approaching to a MIS sample with patterned nanopillars for *in situ* RS characterization. Schematic of MIM cells made using two metallic probes, one of them coated (c), and ultra thin insulating membranes where the electrodes and dielectrics are arranged planar (d) or slanted (e). (a) is reproduced with permission from Ref. [19], copyright Springer Nature 2014. (b) is reproduced with permission from Ref. [11], copyright Wiley-VCH, 2015. (c) is reproduced with permission from Ref. [19], copyright Springer Nature 2014. (d) is reproduced with permission from Ref. [236], copyright IEEE 2016. (e) is reproduced with permission from Ref. [237], copyright 2015.

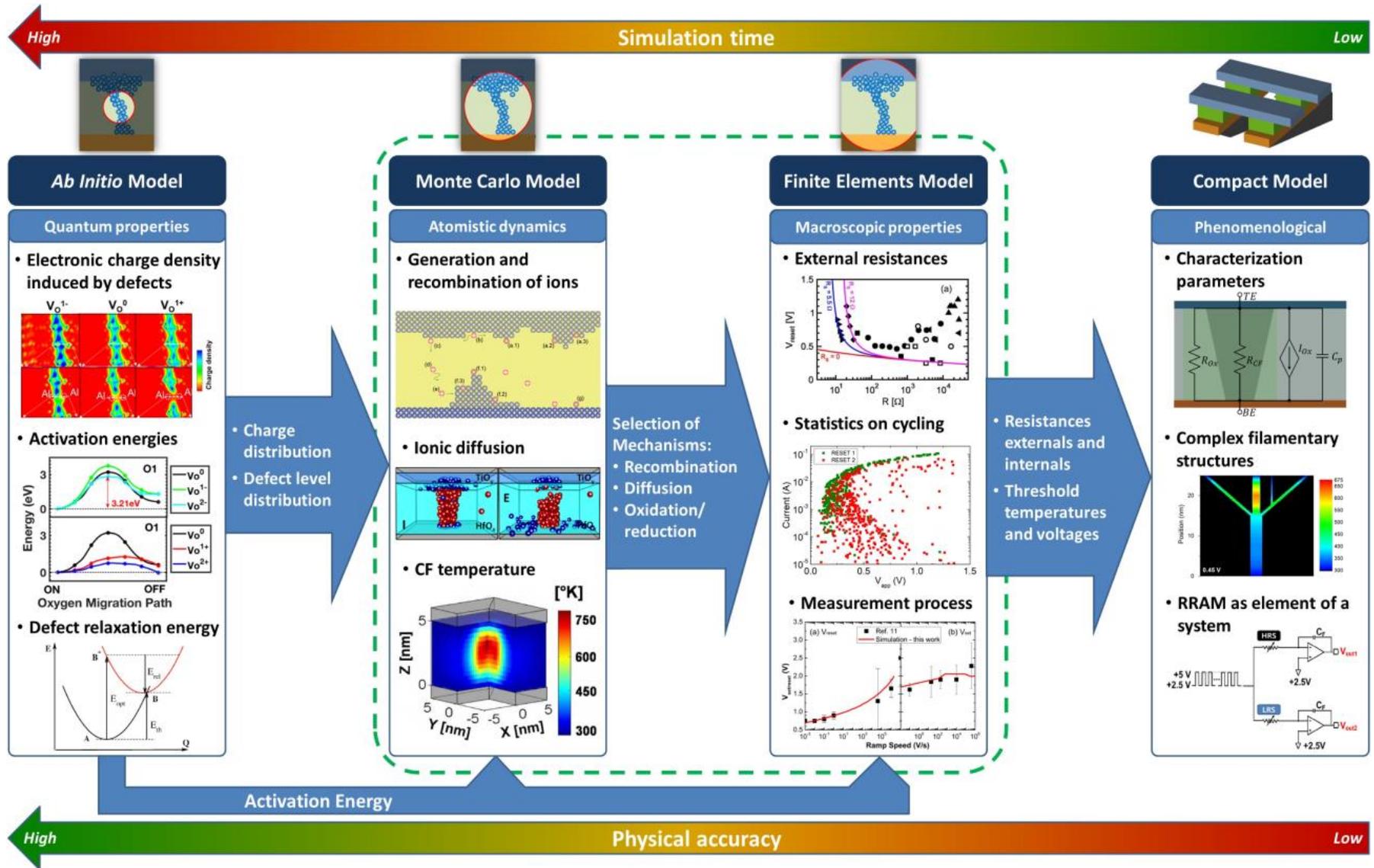


Figure 11 (see caption in the next page)

Figure 11: Schematics on the simulation models used for RRAM device characterization, describing the provided information level and detail. In multiscale approaches the information provided by a higher level model is transferred and embedded in the approximations used by the other models. The choice of a model is routinely determined by the agreement between the physical accuracy needed and the available simulation time. The figures shown in the Ab Initio Model section are for Al:HfO<sub>2</sub> and have been reprinted with permission from Ref. [238], copyright IEEE 2017 and Ref. [239], copyright AIP Publishing LLC. 2006. Figures for Monte Carlo Model have been reproduced with permission from (from top to bottom) Ref. [216], copyright Royal Society of Chemistry 2015 and Ref. [240], copyright IEEE Electron Devices Society 2011. In the same way, the figures of Finite elements section have been extracted from Ref. [241] copyright IEEE Electron Devices Society 2011, Ref. [212], copyright AIP Publishing LLC. 2013 and Ref. [242], copyright AIP Publishing LLC. 2011. Finally, the figures for Compact Model have been extracted from Ref. [223] copyright IOP Publishing 2016, Ref. [231] copyright IEEE Electron Devices Society 2015, and Ref. [50], copyright IEEE 2012.